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NASA TECHNICAL MEMORANDUM

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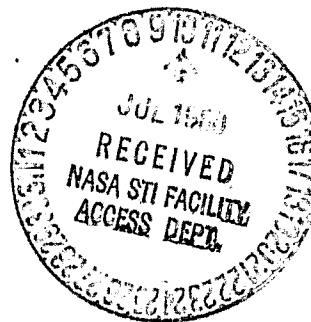
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USERS GUIDE FOR SKYLAB DYNAMICS PROGRAM, SKYDYN

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Systems Dynamics Laboratory

May. 1980



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*George C. Marshall Space Flight Center
Marshall Space Flight Center, Alabama*

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16. ABSTRACT <p>The Skylab Dynamics Program (SKYDYN) is an extensively modified version of the 6-degree-of-freedom digital program REENTR, developed by Northrop Services, Inc., Huntsville, AL. The program REENTR was modified for the Honeywell CP-V System and was tailored to the specific requirements for Skylab.</p> <p>This user's manual provides a description of the capabilities of SKYDYN, the required input data and the resulting program output.</p>					
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TECHNICAL MEMORANDUM

USERS GUIDE FOR SKYLAB DYNAMICS PROGRAM, SKYDYN

I. INTRODUCTION

The program SKYDYN was developed to simulate the orbital dynamics of an uncontrolled asymmetric vehicle subjected to perturbing torques due to gravity gradient and aerodynamic forces. The program utilizes an oblate rotating Earth model and a variable step size, five-pass Runge-Kutta integration scheme. Quaternions are used to represent the attitude of the vehicle; thus, there are no restrictions on attitude or small angle motion.

The versatility of the program output allows the user to specify the output parameters without reprogramming. Tape output can be used for plotting or as input to other programs for open-loop calculations that would otherwise increase the run time for the dynamics program.

The input data requirements and a sample data input listing are given in Section II. Program output specifications and a sample program printout are given in Section III.

Appendix A presents definitions of the program variables. The reference frames and corresponding transformation are given in Appendix B. The equations of motion used in the simulation are presented in Appendix C. A listing of the main routine, SKYDYN, and all subroutines used are given in Appendix D.

II. INPUT DATA REQUIREMENTS

A. Data Input

Table 1 defines the variables required as input to the program SKYDYN. A change in code number indicates the beginning of a new line of input. Each variable specified to be printed and/or saved on tape (see Code 2) begins a new line of input with a maximum of 90 lines per run.

All angular data are input in degrees and converted to radians at the start of each simulation. A more detailed description of the table input for density and aerodynamic coefficients is presented following the list of input data requirements. The transformation matrix from principal to body axes (Code 25) is used for open-loop calculations only, and if data are unavailable, dummy variables may be used as input.

All data listed in Table 1 are required for initialization of the program. If it is desired to restart the simulation with initial conditions saved from a previous run (IOPT1=1), card input data for Codes 23 and 24, the initial start time and integration step size are ignored. For multiple cases (NCASE > 1, Code 1), data cards Codes 17 through 25 are repeated. Card input data are assigned to Unit 5. Tape input (see IOPT1, Code 19) is assigned to Unit 14.

A typical data input listing is given in Section II. D.

TABLE 1. SKYDYN INPUT

<u>Code</u>	<u>Program Symbol</u>	<u>Variable Definition</u>	<u>Units</u>	<u>Format</u>
1	NCASE	Case number	Unitless	I5 (Col 1-5)
	NX	Number of integration variables	Unitless	I5 (Col 6-10)
2	IVAR	Location of variable in common to be printed and/ or saved on tape	Unitless	I3 (Col 1-3)
	ISCAL	Scale factor designation ISCAL=0, Scale factor=1.; ISCAL=1, Scale factor= 57.29578; ISCAL≠0 or ≠1, Scale factor supplied by user.	Unitless	I1 (Col 5)

TABLE 1. (Continued)

<u>Code</u>	<u>Program Symbol</u>	<u>Variable Definition</u>	<u>Units</u>	<u>Format</u>
	SCAL	Scale factor	User Specified	E12.5 (Col 7-18)
	PNAME	Name to be assigned to printed variables	Unitless	A4 (Col 19-22)
	IPW	Print and/or save designation: =0, print and save; =1, print only; =2 save only	Unitless	I1 (Col 23)
3		Blank card to signify end of output variables		
4	ATNM(I) I=1,18	Atmosphere Title Card	Unitless	18A4
5	TLAT(I) I=1,11	Latitude table for density lookup	deg	7F8.3
6	TLNG(I) I=1,37	Longitude table for density lookup	deg	7F8.3
7	FRHO(I,J) I=1,11 J=1,37	Atmospheric density	kg/m ³	6E9.3
8	NALP	Number of total angle-of- attack values	Unitless	I5 (Col 1-5)
	NPHIA	Number of aerodynamic roll angle values	Unitless	I5 (Col 6-10)
9	TALP(I) I=1,NALP	Total angle-of-attack table for aerodynamic data lookup	deg	7F8.3
10	TPHIA(I) I=1,NPHIA	Aerodynamic roll angle table for aerodynamic data lookup	deg	7F8.3
11	FCA(I,J) I=1,NPHIA J=1,NALP	Axial force coefficient	Unitless	7F8.3
12	FCN(I,J) I=1,NPHIA J=1,NALP	Normal force coefficient	Unitless	7F8.3
13	FCY(I,J) I=1,NPHIA J=1,NALP	Side force coefficient	Unitless	7F8.3

TABLE 1. (Continued)

<u>Code</u>	<u>Program Symbol</u>	<u>Variable Definition</u>	<u>Units</u>	<u>Format</u>
14	FCM(I,J) I=1,NPHIA J=1,NALP	Pitching moment coefficient	Unitless	7F8.3
15	FCEN(I,J) I=1,NPHIA J=1,NALP	Yawing moment coefficient	Unitless	7F8.3
16	FCL(I,J) I=1,NPHIA J=1,NALP	Rolling moment coefficient	Unitless	7F8.3
17	CASE(I) I=1,18	Case title card	Unitless	18A4
18	PROPT	Multiplier for print interval (Print interval=PROPT*DTP)	Unitless	F10.1
19	DT	Initial integration time step	sec	F10.4
	DTP	Output frequency for save tape	sec	F10.4
	DTSAM	Specified time to save variables for restart	sec	F10.4
	TRUN	Total run time	sec	F10.4
	TIME	Initial start time	sec	F10.4
	IOPT1	Initialization option =0, use initial conditions from data pack =1, read in initial conditions from tape	Unitless	I5
20	WT	Vehicle weight	lb	F10.4
	XCG	Vehicle cg in x-direction	ft	F10.4
	YCG	Vehicle cg in y-direction	ft	F10.4
	ZCG	Vehicle cg in z-direction	ft	F10.4
	XMRP	Aerodynamic moment reference point in x-direction	ft	F10.4
	YMRP	Aerodynamic moment reference point in Y-direction	ft	F10.4
	ZMRP	Aerodynamic moment reference point in z-direction	ft	F10.4

TABLE 1. (Continued)

<u>Code</u>	<u>Program Symbol</u>	<u>Variable Definition</u>	<u>Units</u>	<u>Format</u>
21	DREF	Aerodynamic reference diameter	ft	F10.4
	SREF	Aerodynamic reference area	ft ²	F10.4
22	IXYZ(1,1)	Moment of inertia about x-axis	slugs-ft ²	F10.1
	IXYZ(2,2)	Moment of inertia about y-axis	slugs-ft ²	F10.1
	IXYZ(3,3)	Moment of inertia about z-axis	slugs-ft ²	F10.1
	IXYZ(1,2)	xy product of inertia	slugs-ft ²	F10.1
	IXYZ(1,3)	xz product of inertia	slugs-ft ²	F10.1
	IXYZ(2,3)	yz product of inertia	slugs-ft ²	F10.1
23	PSI	Geocentric latitude (positive north and negative south of equator)	deg	F10.6
	LAMDE	Earth fixed longitude (positive east and negative west of Greenwich)	deg	F10.5
	RMAG	Radius vector magnitude	ft	F10.2
	VIMAG	Inertial velocity	ft/sec	F10.3
	SIGI	Inertial heading (positive clockwise from north)	deg	F10.6
	GAMI	Inertial flight path angle (positive up from local geocentric horizontal)	deg	F10.8
24	PHIBI	Initial bank angle	deg	F10.5
	ALPHAI	Initial total angle-of-attack	deg	F10.5
	PHIAI	Initial aerodynamic roll angle	deg	F10.5

TABLE 1. (Continued)

<u>Code</u>	<u>Program Symbol</u>	<u>Variable Definition</u>	<u>Units</u>	<u>Format</u>
	PQR(I) I=1,3	Initial rates about x, y, and z body axes, respectively	deg/sec	3F10.5
25	ABP(I,J) J=1,3 I=1,3	Transformation matrix from principal axes to body axes	Unitless	610.5
26		Blank card to signify termination of input data		

B. Density Table Input

The density table input is a bivariate function of latitude (ψ) and longitude (λ). The density values were determined for a specified altitude using the Jacchia 1970-3 atmosphere model and predicted solar and geomagnetic data provided by Space Sciences Laboratory, Marshall Space Flight Center.

The dependent density values are input in the following manner:

$\rho(\psi_1, \lambda_1) \rho(\psi_2, \lambda_1) \dots \dots \dots \rho(\psi_6, \lambda_1)$

$\rho(\psi_7, \lambda_1) \dots \dots \dots \rho(\psi_{11}, \lambda_1)$

$\begin{matrix} \cdot \\ \cdot \\ \cdot \\ \cdot \end{matrix} \qquad \qquad \qquad \begin{matrix} \cdot \\ \cdot \\ \cdot \\ \cdot \end{matrix}$

$\rho(\psi_1, \lambda_{37}) \rho(\psi_2, \lambda_{37}) \dots \dots \dots \rho(\psi_6, \lambda_{37})$

$\rho(\psi_7, \lambda_{37}) \dots \dots \dots \rho(\psi_{11}, \lambda_{37})$

C. Aerodynamic Coefficients Table Input

The aerodynamic coefficients are bivariate functions of aerodynamic roll angle (ϕ_w) and total angle-of-attack (α_T). The dimension of these tables is chosen by the user with the restriction that all six coefficients must have the same dimension.

For the sample case presented, the coefficients are dimensioned 21 \times 11 and are input in the following manner:

$C(\phi_{\alpha 1}, \alpha_{T1})$	$C(\phi_{\alpha 7}, \alpha_{T1})$
$C(\phi_{\alpha 8}, \alpha_{T1})$	$C(\phi_{\alpha 14}, \alpha_{T1})$
$C(\phi_{\alpha 15}, \alpha_{T1})$	$C(\phi_{\alpha 21}, \alpha_{T1})$
⋮		⋮
$C(\phi_{\alpha 1}, \alpha_{T11})$	$C(\phi_{\alpha 7}, \alpha_{T11})$
⋮		⋮
$C(\phi_{\alpha 15}, \alpha_{T11})$	$C(\phi_{\alpha 21}, \alpha_{T11})$

D. Sample Data Input Listing

1	13
667	THORO
008	OSQR1
151 1	PH180
152 1	ALPT0
153 1	PH1A0
503	VRELI
002	DELT1
329 1	CAMR1
328 1	SIGR1
517	VELX1
518	VELY1
519	VELZ1
061 1	P 0
021 1	POOT1
526	GC810
431	TOAX0
532	TABX0
410	CAR10
062 1	Q 0
022 1	QOOT1
527	GC820
432	TOAY0
533	TABY0
411	CAR21
063 1	R 0
023 1	ROOT1
528	GC830
433	TOAZ0
534	TABZ0
412	CAR31
154	BR110
155	BR210
156	BR310
157	BR120
158	BR220
159	BR320
160	BR130
161	BR230
162	BR330
181	I8111
182	I8211
183	I8311
184	I8121
185	I8221
186	I8321
187	I8131
188	I8231
189	I8331
501	RHO 1

502
323 1
326 1
331 1
330 1

QBARI
LAT 1
LONG 1
CART 1
SIGH 1

SSL SENSITIVITIES, P (LAT, LONG), 230NM, MEASURED

	-40.	-30.	-20.	-10.	0.	10.
20.	30.	40.	50.			60.
0.	10.	20.	30.	40.	50.	60.
70.	80.	90.	100.	110.	120.	130.
140.	150.	160.	170.	180.	190.	200.
210.	220.	230.	240.	250.	260.	270.
280.	290.	300.	310.	320.	330.	340.
350.	360.					
270E-11	296E-11	321E-11	345E-11	365E-11	381E-11	391E-11
392E-11	397E-11	396E-11	388E-11	376E-11		
268E-11	293E-11	318E-11	341E-11	361E-11	377E-11	377E-11
389E-11	393E-11	392E-11	385E-11	373E-11		
263E-11	287E-11	311E-11	333E-11	352E-11	367E-11	367E-11
378E-11	383E-11	383E-11	377E-11	366E-11		
295E-11	277E-11	299E-11	319E-11	337E-11	352E-11	352E-11
362E-11	367E-11	368E-11	364E-11	355E-11		
245E-11	265E-11	284E-11	302E-11	319E-11	332E-11	332E-11
342E-11	348E-11	349E-11	347E-11	341E-11		
342E-11	250E-11	267E-11	283E-11	298E-11	310E-11	310E-11
319E-11	325E-11	328E-11	328E-11	325E-11		
221E-11	235E-11	249E-11	263E-11	275E-11	286E-11	286E-11
295E-11	301E-11	306E-11	308E-11	307E-11		
209E-11	220E-11	232E-11	243E-11	253E-11	262E-11	262E-11
271E-11	278E-11	283E-11	287E-11	290E-11		
197E-11	205E-11	214E-11	223E-11	232E-11	240E-11	240E-11
240E-11	255E-11	262E-11	268E-11	273E-11		
188E-11	192E-11	198E-11	205E-11	212E-11	219E-11	219E-11
226E-11	234E-11	241E-11	249E-11	257E-11		
176E-11	179E-11	184E-11	189E-11	195E-11	201E-11	201E-11
207E-11	215E-11	223E-11	233E-11	243E-11		
167E-11	168E-11	172E-11	175E-11	179E-11	184E-11	184E-11
191E-11	198E-11	208E-11	218E-11	230E-11		
159E-11	159E-11	161E-11	164E-11	167E-11	171E-11	171E-11
177E-11	185E-11	194E-11	206E-11	220E-11		
153E-11	152E-11	153E-11	154E-11	157E-11	160E-11	160E-11
166E-11	174E-11	184E-11	196E-11	211E-11		
148E-11	146E-11	146E-11	147E-11	149E-11	152E-11	152E-11
157E-11	165E-11	175E-11	188E-11	204E-11		
145E-11	142E-11	141E-11	142E-11	143E-11	146E-11	146E-11
151E-11	159E-11	169E-11	183E-11	199E-11		
142E-11	139E-11	138E-11	136E-11	139E-11	142E-11	142E-11
147E-11	155E-11	165E-11	179E-11	196E-11		
141E-11	138E-11	136E-11	136E-11	137E-11	140E-11	140E-11
145E-11	153E-11	163E-11	177E-11	194E-11		
141E-11	137E-11	136E-11	136E-11	136E-11	139E-11	139E-11

ORIGINAL PAGE IS
OF POOR QUALITY

.144E-11	.152E-11	.162E-11	.176E-11	.193E-11	
.140E-11	.137E-11	.136E-11	.135E-11	.136E-11	.139E-11
.144E-11	.151E-11	.162E-11	.176E-11	.193E-11	
.140E-11	.137E-11	.136E-11	.136E-11	.136E-11	.139E-11
.144E-11	.152E-11	.162E-11	.176E-11	.193E-11	
.141E-11	.138E-11	.136E-11	.136E-11	.137E-11	.140E-11
.145E-11	.152E-11	.163E-11	.177E-11	.194E-11	
.142E-11	.139E-11	.138E-11	.138E-11	.139E-11	.142E-11
.147E-11	.154E-11	.165E-11	.179E-11	.195E-11	
.145E-11	.142E-11	.141E-11	.142E-11	.143E-11	.146E-11
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.149E-11	.147E-11	.147E-11	.148E-11	.150E-11	.153E-11
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.155E-11	.154E-11	.155E-11	.157E-11	.159E-11	.163E-11
.169E-11	.177E-11	.187E-11	.199E-11	.213E-11	
.163E-11	.164E-11	.166E-11	.169E-11	.173E-11	.178E-11
.184E-11	.191E-11	.201E-11	.212E-11	.225E-11	
.173E-11	.176E-11	.181E-11	.185E-11	.190E-11	.196E-11
.203E-11	.210E-11	.219E-11	.229E-11	.240E-11	
.165E-11	.191E-11	.198E-11	.205E-11	.212E-11	.218E-11
.226E-11	.233E-11	.241E-11	.249E-11	.257E-11	
.199E-11	.208E-11	.218E-11	.227E-11	.236E-11	.244E-11
.252E-11	.259E-11	.266E-11	.271E-11	.276E-11	
.214E-11	.226E-11	.239E-11	.251E-11	.262E-11	.272E-11
.280E-11	.287E-11	.292E-11	.296E-11	.297E-11	
.229E-11	.244E-11	.260E-11	.275E-11	.288E-11	.300E-11
.309E-11	.315E-11	.319E-11	.320E-11	.313E-11	
.242E-11	.261E-11	.280E-11	.298E-11	.313E-11	.326E-11
.336E-11	.342E-11	.344E-11	.342E-11	.337E-11	
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.268E-11	.294E-11	.318E-11	.341E-11	.362E-11	.377E-11
.388E-11	.393E-11	.392E-11	.385E-11	.373E-11	
.270E-11	.296E-11	.321E-11	.345E-11	.365E-11	.381E-11
.392E-11	.397E-11	.396E-11	.388E-11	.376E-11	
11	21				
0.0	20.0	40.0	60.0	80.0	90.0 100.0
120.0	140.0	160.0	180.0		
0.0	20.0	40.0	50.0	80.0	90.0 100.0
120.0	140.0	160.0	180.0	200.0	220.0 240.0
260.0	270.0	280.0	300.0	320.0	340.0 360.0
2.401	2.401	2.401	2.401	2.401	2.401 2.401
2.401	2.401	2.401	2.401	2.401	2.401 2.401
2.401	2.401	2.401	2.401	2.401	2.401 2.401
3.166	3.129	2.964	2.787	2.600	2.707 2.517
2.952	3.340	3.630	3.860	3.554	3.212 2.798
2.370	2.625	2.576	2.842	2.945	3.099 3.166
4.124	3.919	3.330	3.036	2.669	2.687 2.710
3.522	4.202	4.713	4.873	4.672	3.909 3.063
2.486	2.628	2.706	3.286	3.699	4.145 4.124

3.366	3.251	2.989	2.560	2.110	1.988	2.154
2.854	3.423	3.857	4.017	3.840	3.187	2.473
1.980	1.988	2.164	2.828	3.187	3.407	3.366
1.433	1.347	1.220	.997	.812	.741	.832
1.122	1.315	1.471	1.518	1.436	1.224	.976
.786	.763	.847	1.125	1.290	1.371	1.433
.001	-.004	-.001	.003	.004	.004	.004
.004	.004	.005	.005	.005	.004	.005
.005	.005	.005	.004	-.001	-.003	.001
-1.529	-1.445	-1.226	-.993	-.801	-.730	-.827
-1.128	-1.317	-1.399	-1.446	-1.359	-1.225	-.974
-.779	-.754	-.839	-1.130	-1.323	-1.492	-1.529
-4.142	-3.905	-3.332	-2.725	-2.111	-1.988	-2.186
-2.943	-3.298	-3.566	-3.515	-3.321	-2.767	-2.419
-1.999	-2.049	-2.204	-2.987	-3.535	-3.971	-4.142
-5.136	-4.899	-4.366	-3.591	-2.760	-2.742	-2.810
-3.513	-3.581	-4.308	-4.308	-3.882	-3.255	-2.962
-2.595	-2.829	-2.868	-3.769	-4.533	-4.956	-5.136
-4.106	-3.966	-3.491	-3.201	-2.700	-2.813	-2.630
-3.044	-3.209	-3.313	-3.344	-3.246	-3.029	-2.901
-2.556	-2.858	-2.760	-3.299	-3.646	-4.007	-4.106
-2.590	-2.590	-2.590	-2.590	-2.590	-2.590	-2.590
-2.590	-2.590	-2.590	-2.590	-2.590	-2.590	-2.590
-2.590	-2.590	-2.590	-2.590	-2.590	-2.590	-2.590
.002	.002	.002	.002	.002	.002	.002
.002	.002	.002	.002	.002	.002	.002
.002	.002	.002	.002	.002	.002	.002
1.314	1.225	.960	.609	.227	-.001	-.224
-.663	-1.096	-1.434	-1.618	-1.404	-1.058	-.632
-2.12	-.006	-.235	-.624	-.951	-1.208	-1.314
3.770	3.372	2.366	1.419	.468	-.001	-.472
-1.655	-2.953	-4.022	-4.416	-3.989	-2.759	-1.456
-.440	.010	.493	1.548	2.625	3.566	3.770
6.235	5.657	4.279	2.415	.733	-.001	-.751
-2.691	-4.853	-6.658	-7.368	-6.629	-4.532	-2.357
-.702	-.009	-.780	-2.678	-4.558	-5.923	-6.235
8.578	7.626	5.647	3.026	.903	.000	-.933
-3.422	-6.029	-8.215	-8.985	-8.015	-5.615	-2.993
-.893	.004	.976	3.436	5.971	7.762	8.578
9.330	8.237	5.874	3.115	.922	.000	-.961
-3.578	-6.320	-8.339	-9.236	-8.203	-5.902	-3.149
-.935	.001	-1.009	-3.584	-6.291	-8.460	-9.330
9.153	8.132	5.659	3.040	.900	.000	-.938
-3.465	-6.069	-7.853	-8.640	-7.625	-5.655	-3.020
-.900	.003	.981	3.479	6.114	8.393	9.153
7.605	6.757	4.746	2.578	.734	.000	-.768
-2.778	-4.661	-6.146	-6.438	-5.715	-3.928	-2.312
-.717	.007	-.800	-2.838	-5.037	-6.867	-7.605
4.644	4.181	3.073	1.695	.491	.000	-.500
-1.643	-2.777	-3.668	-3.886	-3.295	-2.281	-1.406
-.468	.006	.526	1.785	3.189	4.224	4.644
1.703	1.552	1.143	.716	.248	-.001	-.246

-678	-1.041	-1.298	-1.390	-1.271	-982	-649
-239	-002	.257	.739	1.189	1.566	1.703
-000	-000	-000	-000	-000	-000	-000
-000	-000	-000	-000	-000	-000	-000
-000	-000	-000	-000	-000	-000	-000
-002	-002	-002	-002	-002	-002	-002
-002	-002	-002	-002	-002	-002	-002
-002	-002	-002	-002	-002	-002	-002
-000	-008	-1.724	-929	-994	-1.040	-966
-985	-021	-473	-001	.460	.779	.520
-090	1.005	.977	.943	.720	.405	.000
-000	-1.113	-1.040	-2.280	-2.295	-2.346	-2.330
-2.037	-2.322	1.304	-001	1.360	2.137	2.264
2.100	2.269	2.307	2.457	2.033	1.209	-000
-000	-1.947	-3.375	-3.931	-3.711	-3.551	-3.778
-4.367	-3.876	-2.320	-001	2.307	3.585	3.748
3.445	3.516	3.775	4.321	3.589	2.037	-000
-000	-2.640	-4.490	-4.959	-4.615	-4.280	-4.721
-5.576	-4.840	-2.876	-001	2.007	4.482	4.809
4.423	4.360	4.776	5.568	4.740	2.686	-000
-000	-2.857	-4.670	-5.103	-4.715	-4.348	-4.857
-5.026	-5.072	-2.923	-001	2.875	4.714	5.065
4.626	4.515	4.945	5.806	4.990	2.933	-000
-000	-2.021	-4.495	-4.973	-4.609	-4.269	-4.734
-5.637	-4.871	-2.754	-001	2.674	4.510	4.832
4.431	4.359	4.780	5.628	4.846	2.911	-000
-000	-2.335	-3.752	-4.169	-3.703	-3.545	-3.825
-4.494	-3.731	-2.148	-001	1.999	3.114	3.659
3.464	3.615	3.834	4.548	3.973	2.374	-000
-000	-1.426	-2.388	-2.663	-2.348	-2.372	-2.392
-2.613	-2.194	-1.264	-001	1.136	1.778	2.179
2.186	2.424	2.421	2.784	2.476	1.442	-000
-000	-505	-840	-1.043	-1.011	-1.066	-980
-998	-783	-429	-002	.418	.733	.940
.951	1.074	1.027	1.070	.874	.510	.000
-001	-001	-001	-001	-001	-001	-001
-001	-001	-001	-001	-001	-001	-001
-001	-001	-001	-001	-001	-001	-001
-332	-332	-332	-332	-332	-332	-332
-332	-332	-332	-332	-332	-332	-332
-332	-332	-332	-332	-332	-332	-332
-1.578	-1.492	-1.249	-937	-497	-317	-150
-030	.075	.169	.335	.116	.009	-086
-175	-339	-516	-951	-1.235	-1.468	-1.578
-3.628	-3.294	-2.490	-1.632	-.695	-.269	-.080
.606	1.117	1.598	1.784	1.568	.832	.346
.037	-.292	-.729	-1.774	-2.778	-3.533	-3.628
-6.041	-4.677	-3.778	-2.263	-.074	-.192	-.355
1.525	2.804	3.719	4.023	3.678	2.383	1.082
.277	-.203	-.935	-2.577	-4.119	-5.011	-5.041
-6.132	-5.639	-4.170	-2.280	-.928	-.068	-.652
2.423	4.102	5.471	5.782	5.210	3.532	1.020

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.594	-.069	-.925	-2.845	-4.627	-5.930	-6.132
-6.423	-5.807	-4.045	-2.124	-.730	.000	-.785
2.755	4.593	5.990	6.378	5.757	4.025	2.166
.747	-.001	-.846	-2.772	-4.629	-6.051	-6.423
-5.767	-5.251	-3.564	-1.858	-.593	.068	.872
2.875	-4.740	5.988	6.346	5.740	4.192	2.317
.833	.061	-.708	-2.469	-4.171	-5.535	-5.767
-4.302	-3.842	-2.578	-1.353	-.329	.193	.904
2.722	4.323	5.358	5.334	4.938	3.662	2.292
.884	.177	-.426	-1.721	-2.977	-4.008	-4.302
-2.161	-1.895	-1.326	-.693	-.155	.265	.735
1.923	3.011	3.712	3.821	3.383	2.585	1.727
.732	.246	-.201	-.824	-1.462	-1.933	-2.161
-.487	-.419	-.199	-.089	.091	.305	.518
1.035	1.376	1.648	1.731	1.630	1.318	1.013
.518	.297	.076	-.122	-.260	-.439	-.487
.304	.304	.304	.304	.304	.304	.304
.304	.304	.304	.304	.304	.304	.304
-.298	-.298	-.298	-.298	-.298	-.298	-.298
-.298	-.298	-.298	-.298	-.298	-.298	-.298
-.298	-.298	-.298	-.298	-.298	-.298	-.298
-.421	-.143	.121	.527	.728	.706	.788
.663	-.413	-.038	-.536	-.665	-.824	-.908
-.836	-1.134	-1.050	-1.006	-.827	-.651	-.421
-.719	.115	.910	1.583	2.049	2.062	2.061
1.926	1.379	.449	-.686	-1.590	-1.830	-1.769
-1.836	-2.149	-2.227	-2.271	-1.954	-1.522	-.719
-.522	.879	1.971	2.744	3.243	3.221	3.280
3.279	2.552	1.121	-.674	-2.284	-3.015	-2.788
-2.874	-3.251	-3.410	-3.671	-3.120	-1.972	-.522
-.244	1.625	2.925	3.434	3.899	3.865	4.032
4.279	3.427	1.839	-.264	-2.234	-3.302	-3.403
-3.664	-4.011	-4.168	-4.481	-3.656	-2.132	-.244
-.001	2.041	3.273	3.606	3.984	3.948	4.181
4.572	-3.735	-2.121	.000	-2.043	-3.252	-3.531
-3.858	-4.164	-4.286	-4.579	-3.723	-2.125	-.001
.291	2.253	3.345	3.599	3.862	3.844	4.104
4.550	3.798	2.216	.248	-1.687	-2.918	-3.321
-3.698	-3.969	-4.078	-4.287	-3.398	-1.814	.291
.776	2.418	3.301	3.459	3.255	3.257	3.503
3.977	-3.388	-2.146	-.556	-.970	-1.969	-2.657
-3.070	-3.281	-3.291	-3.314	-2.472	-1.034	.776
.943	1.944	2.537	2.638	2.373	2.378	2.422
2.634	2.316	1.662	.767	-.230	-.983	-1.575
-2.037	-2.117	-2.080	-1.846	-1.191	-.192	.943
.731	1.112	1.261	1.356	1.225	1.350	1.125
1.218	1.096	-.846	-.519	-.136	-.138	-.501
-.745	-.659	-.690	-.519	-.137	.270	.731
.436	.436	.436	.436	.436	.436	.436
.436	.436	.436	.436	.436	.436	.436
.436	.436	.436	.436	.436	.436	.436

SAMPLE CASE									
100.	14.0	50.0	71900.0	72000.0	0.0	0.0	0.0	0.0	0.0
157710.	-27.28	-0.325	2.64	0.0	0.0	0.0	0.0	0.0	0.0
33.	855.3006								
6322989.	2870412.	2751954.	45813.	391287.	19334.				
0.	0.	22323228.	25120.315	40.	0.				
-92.	86.7774	270.	1.73623	-0.05752	1.2772				
-9841605	-0162073		1765375	-0210063	9781355				
1760309	-2073364	.9623018							

III. PROGRAM OUTPUT

A. Output Specifications

The program allows the user to specify up to 90 variables, contained in the first 999 locations of the common block, for printing or to be saved on tape. Printed output data are assigned to Unit 6. Each block of printed data are preceded by the simulation time and case title. The block of printed data (6 variables per line of print) uses an E15.8 format with a four character identification name.

All tape output data are written in binary form. Variables saved for restart are assigned to Unit 13. Data to be plotted or used as input to other programs are assigned to Unit 12. The first variable of the data block saved is the simulation time in seconds. The remaining variables, and their order of output, are specified by the input data (See Section III, Code 2).

B. Sample Program Printout

SAMPLE CASE

CASE NUMBER 1

*****VEHICLE DATA*****

WEIGHT = 157710.000
 MOMENT REFERENCE POINT = (.0000, .0000, .0000)
 AERODYNAMIC REFERENCE LENGTH = 33.0000
 AERODYNAMIC REFERENCE AREA = 855.3006

VEHICLE INERTIA MATRIX =
 -45813.0 -391287.0 -391287.0
 -391287.0 -391287.0 -19334.0
 -19334.0 2751954.0

*****INITIAL CONDITIONS*****

RHAC = 22323228.
 GEOCENTRIC LATITUDE = .000000
 LONGITUDE = .00300
 INERTIAL VELOCITY = 25120.315
 INERTIAL HEADING = 40.0000
 INERTIAL FLIGHT PATH ANGLE = .000000

VEHICLE ATTITUDE DATA -
 PHIBI +1 = -92.00000
 ALPHAI +2 = 88.77740
 PHIAI +1 = 270.00000

INITIAL BODY RATES
 ROLL RATE = 1.73623
 PITCH RATE = -.05752
 YAW RATE = .12772

ABP
 .9841605E 00 .1620730E 01 .1765375E 00
 .2100639E 01 .9781355E 00 .2069051E 00
 .1760309E 00 .2073364E 00 .9623018E 00

*****OTHER INFORMATION*****

THIS PROGRAM USES SSL DENSITIES, F(LAT, LONG), 230NM, MEASURED

DELT 14.00000 DTFR 50.00000 DTSM 71900.00 TRUN 72000.00 TIME .00 IOPT 0

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TIME .00000000E 00 SAMPLE CASE

THOR .00000000E 00 QSOR .10000000E 01 PHIB-.92000001E 02 ALPT .80777401E 02 PHIA .27000000E 03 VREL .24106222E 05
DELT .14000000E 02 CAMR .50330791E-24 S1CR .37034776E-03 VELX .51434911E 03 VELY .24100726E 05 VELZ .61097015E 06
P .17362300E 01 PDOT .29179373E-03 GGB1 .67537424E-01 TOAX .19997458E-03 TABX .67337449E-01 CAR1 .44971102E 01
Q .57520600E-01 QDOT .42798320E-02 GGB2 .12011496E 01 TOAY .22367242E-04 TABY .12011719E-01 CAR2 .13059337E-02
R .17723000E 00 RDOT .22653979E-02 GGB3 .14629498E-02 TOAZ .25052432E-04 TABZ .30814558E 01 CAR3 .21595551E 00
BR11 .21336776E-01 BR21 .99916331E 00 BR31 .34891552E-01 BR12 .34091723E 00 BR22 .21323778E-01 BR32 .17444249E-02
BR13 .25345245E-09 BR23 .34899497E-01 BR33 .99939083E 00 BR14 .74464743E-03 BR24 .74464743E-03 BR34 .99939083E 00
BR15 .78475105E 00 BR25 .27859224E-01 BR35 .61082822E 00 BR16 .78524506E 00 BR26 .78524506E 00 BR36 .21019958E-01
RHC .71727339E-14 QBAR .21420701E-05 LAT .00000000E 00 LONI .00000000E 00 CAMI .48239870E-24 S1CI .40000000E 02

TIME .50460000E 04 SAMPLE CASE

THOR .14000000E 01 QSOR .10000039E 01 PHIB-.14047984E 03 ALPT .10656796E 03 PHIA .31927640E 03 VREL .24091804E 05
DELT .14000000E 02 CAMR .83026439E-01 S1CR .43189544E 02 VELX .68698884E 04 VELY .15065303E 05 VELZ .17500441E 05
P .15769681E 01 PDOT .73576451E-03 GGB1 .59098450E-01 TOAX .79386784E-02 TABX .59823318E 00 CAR1 .25422781E 01
Q .29990150E 00 QDOT .11259377E-02 GGB2 .19439304E 01 TOAY .39763889E-01 TABY .19836943E 01 CAR2 .25659871E 00
R .43336474E 00 RDOT .42785581E-02 GGB3 .37751404E 01 TOAZ .31983303E-01 TABZ .37431571E 01 CAR3 .10902362E-01
BR11 .28515458E 00 BR21 .50109348E 00 BR31 .81706463E 00 BR12 .84533506E 00 BR22 .54878170E 00 BR32 .55480011E 00
BR13 .72640643E 00 BR23 .66914806E 00 BR33 .15685382E 00 BR14 .81173253E-01 BR24 .81173253E-01 BR34 .52643165E 00
BR15 .23265300E 00 BR25 .94539474E 00 BR35 .47915756E 00 BR16 .31565889E 00 BR26 .31565889E 00 BR36 .81902140E 00
RHC .69555831E-14 QBAR .17573757E-05 LAT .25984655E 02 LONI .35561530E 03 CAMI .19934758E-01 S1CI .45625149E 02

TIME .10080000E 05 SAMPLE CASE

THOR .28000000E 01 QSOR .10000079E 01 PHIB-.55653710E 02 ALPT .93810592E 02 PHIA .31534739E 02 VREL .24067797E 05
DELT .14000000E-02 CAMR .53289897E-01 S1CR .66409990E-02 VELX .15995385E-04 VELY .12560254E-05 VELZ .20468605E 05
P .17174721E 01 PDOT .83596535E-03 GGB1 .54336834E 00 TOAX .62465101E-01 TABX .48090324E 00 CAR1 .78386424E 01
Q .16706133E 00 QDOT .10221147E-02 GGB2 .21335679E 01 TOAY .34285019E-01 TABY .21678538E 01 CAR2 .16832387E 00
R .25983901E 00 RDOT .50209526E-02 GGB3 .30950126E 01 TOAZ .13556832E-01 TABZ .30814558E 01 CAR3 .21595551E 00
BR11 .66459686E-01 BR21 .82383186E 00 BR31 .56295585E 00 BR12 .52186970E 00 BR22 .45218628E 00 BR32 .72333376E 00
BR13 .85045610E 00 BR23 .34187357E 00 BR33 .39987746E 00 BR14 .11030652E 00 BR24 .74867493E 00 BR34 .65372275E 00
BR15 .98880791E 00 BR25 .16072869E-01 BR35 .14843419E 00 BR16 .10063051E 00 BR26 .66276666E 00 BR36 .74202022E 00
RHC .42199782E-14 QBAR .12222299E-05 LAT .45850138E 02 LONI .29945043E 03 CAMI .18323906E-01 S1CI .67444995E 02

TIME .15120000E 05 SAMPLE CASE

THOR .42000000E 01 QSOR .10000119E 01 PHIB-.64085556E 02 ALPT .12164011E 03 PHIA .94233077E 02 VREL .24067260E 05
DELT .14000000E 02 CAMR .53421578E-01 S1CR .10721627E 03 VELX .12625363E 05 VELY .20434181E 05 VELZ .15124531E 04
P .17108091E 01 PDOT .86864621E-03 GGB1 .24130842E-01 TOAX .15912015E-02 TABX .22539641E-01 CAR1 .41579238E 01
Q .22888160E 00 QDOT .11841670E-02 GGB2 .17522241E 01 TOAY .14564135E-02 TABY .17536805E 01 CAR2 .32635276E-01
R .25570274E 00 RDOT .46911601E-02 GGB3 .30446808E 00 TOAZ .77407063E-02 TABZ .31220931E 00 BR32 .16224456E 00
BR11 .52458663E 00 BR21 .76570108E 00 BR31 .37207220E 00 BR12 .84909478E 00 BR22 .50280950E 00 BR32 .16224456E 00
BR13 .62842761E-01 BR23 .40104102E 00 BR33 .91395269E 00 BR14 .60255642E 00 BR24 .77832291E 00 BR34 .17514531E 00
BR15 .73231543E 00 BR25 .62706959E 00 BR35 .31650678E 00 BR16 .31857627E-01 BR26 .31857627E-01 BR36 .94810399E 00
RHC .29635062E-14 QBAR .85828028E-06 LAT .47867339E 02 LONI .24737058E 03 CAMI .10900869E-03 S1CI .10647919E 03

TIME .20160000E 05 SAMPLE CASE

THOR .56000000E 01 QSQR .10000159E 01 PHIB-.92602805E 02 ALPT .3425274E 02 PHIA .15911975E 03 VREL .24093032E 05
 DELT .14000000E 02 GAMR .98312027E-01 SIGR .13428372E 03 VELX .19874588E-05 VELY .48548482E 04 VELZ .12726749E 06
 P .16345488E 01 PDOT .72622674E-03 GCB1-.24478415E 00 TOAX-.29721171E-02 TABX-.24775627E 00 CAR1-.55804310E 01
 Q .13251078E 00 QDOT-.34428498E-02 GCB2-.36302376E 00 TOAY-.25061130E-01 TABY-.38808489E 00 CAR2-.37029733E 00
 R .44714938E 00 RDOT .34141259E-02 GCB3-.87371921E 00 TOAZ-.1188536E-01 TABZ .86185068E 00 CAR3 .92113528E-01
 BR11 .82491620E 00 BR21-.56476793E 00 BR31-.20150425E 00 BR12-.20150425E 00 BR22-.33614470E 00 BR32 .92095448E 00
 BR13-.52823358E 00 BR23-.75376000E 00 BR33 .39107676E 00 BR11 .55511788E 00 BR21 .83111308E 00 BR31-.34553815E-01
 BR12-.82166034E 00 BR22-.54035081E 00 BR32-.18635687E 00 BR13-.13620922E 00 BR23-.13179490E 00 BR32 .98192341E 00
 RHO .26316836E-14 QBAR .76381219E-06 LAT -.30025320E 02 LONI .20786087E 03 GANI-.10829239E-01 SIGI .13203963E 03

TIME .25200000E 05 SAMPLE CASE

THOR .76000000E 01 QSQR .10000199E 01 PHIB-.89926058E 02 ALPT .91196217E 02 PHIA .22676562E 03 VREL .24113241E 05
 DELT .14000000E 02 GAMR .20195882E-01 SIGR .14279188E 03 VELX-.50343715E 03 VELY-.17565441E 05 VELZ-.16514895E 05
 P .17391894E 01 PDOT .29290790E-03 GCB1-.23098630E 00 TOAX-.33388075E-01 TABX .19769823E 00 CAR1-.68018946E 01
 Q .83603655E-01 QDOT-.47033452E-02 GCB2-.71178876E 00 TOAY-.14941819E-01 TABY-.72673058E 00 CAR2 .11788410E 01
 R .11138874E 00 RDOT .11908389E-02 GCB3-.66969949E 00 TOAZ .14447640E-01 TABZ .65525185E 00 CAR3-.31058738E 00
 BR11-.26878037E-01 BR21-.99982021E 00 BR31-.12903083E 00 BR12-.72845624E 00 BR22 .14334069E-01 BR32 .68502812E 00
 BR13-.68488906E 00 BR23-.15248602E-01 BR33-.72856833E 00 BR11-.18770412E-01 BR21 .6175713E 00 BR31-.78619451E 00
 BR12-.78512956E 00 BR22 .47780779E 00 BR32 .39419383E 00 BR13 .61911005E 00 BR23 .62465457E 00 BR33 .47605332E 00
 RHO .26629954E-14 QBAR .77419721E-06 LAT -.45909697E 01 LONI .18237691E 03 GANI-.2728454E-02 SIGI .13984665E 03

TIME .30240000E 05 SAMPLE CASE

THOR .84000000E 01 QSQR .10000238E 01 PHIB-.15057682E 03 ALPT .10550746E 03 PHIA .28242493E 03 VREL .24102279E 05
 DELT .14000000E 02 GAMR-.83478081E-01 SIGR .13883130E 03 VELX-.64435305E 04 VELY-.22682484E 05 VELZ-.49974140E 04
 P .16685238E 01 PDOT .27485078E-03 GCB1 .29431738E 00 TOAX-.36509205E-02 TABX .29066646E 00 CAR1-.49371637E 01
 Q .11994295E 00 QDOT .48753305E-02 GCB2 .36294657E 01 TOAY .19398469E-02 TABY .36314056E 01 CAR2 .19840531E 00
 R .50414431E 00 RDOT .20554326E-02 GCB3-.22428856E 01 TOAZ-.18816029E-02 TABZ .22447672E 01 CAR3 .48341630E-01
 BR11-.26738262E 00 BR21-.47341446E 00 BR31-.83938097E 00 BR12-.94109294E 00 BR22-.59140360E-01 BR32-.33315752E 00
 BR13 .20734197E 00 BR23 .87893180E 00 BR33-.42969288E 00 BR11 .83849382E 00 BR21 .17726502E 00 BR31-.51544192E 00
 BR12-.51920151E 00 BR22 .54766614E 00 BR32-.65623092E 00 BR13 .16593085E 00 BR23 .81779353E 00 BR33 .55120629E 00
 RHO .30410736E-14 QBAR .88331002E-06 LAT .21651254E 02 LONI .15872397E 03 GANI .96768489E-02 SIGI .13623389E 03

TIME .35280000E 05 SAMPLE CASE

THOR .98000000E 01 QSQR .10000278E 01 PHIB-.57168979E 02 ALPT .94970126E 02 PHIA .15246622E 03 VREL .24073928E 05
 DELT .14000000E 02 GAMR-.81904632E-01 SIGR .11920856E 03 VELX-.20857588E 04 VELY .63072732E 04 VELZ .23140179E 05
 P .17314916E 01 PDOT .67096724E-03 GCB1-.65834859E 00 TOAX-.60909402E-01 TABX .59743919E 00 CAR1-.87391084E 01
 Q .13844598E 00 QDOT .27343138E-02 GCB2 .12049614E 01 TOAY .40612918E-01 TABY .12455743E 01 CAR2 .93774492E-01
 R .19042582E 00 RDOT .43338830E-02 GCB3-.36304254E 01 TOAZ-.40890499E-02 TABZ .36263363E 01 CAR3-.94384181E 01
 BR11-.86639555E-01 BR21-.83715151E 00 BR31-.54014900E 00 BR12 .26199547E 00 BR22 .50403256E 00 BR32-.82311071E 00
 BR13 .96121126E 00 BR23-.21282291E 00 BR33-.17565346E 00 BR11 .19022277E 00 BR21 .56121353E 00 BR31-.80553104E 00
 BR12-.30754901E 00 BR22 .81338905E 00 BR32-.49397728E 00 BR13 .93237276E 00 BR23 .15375084E 00 BR33-.32728662E 00
 RHO .39717499E-14 QBAR .11509266E-05 LAT .43301751E 02 LONI .12554690E 03 GANI .60318506E-02 SIGI .11789020E 03

Appendix A

PROGRAM VARIABLE DEFINITIONS

The following program variables, located in the COMMON BLOCK, are alphabetized according to their Fortran Mnemonics.

<u>Program Symbol</u>	<u>Variable Definition</u>	<u>Units</u>
ABI(3,3)	Transformation matrix from I to B-frame	Unitless
ACCOM(582)	Dummy common	Unitless
ADG(3,3)	Transformation matrix from G to D-frame	Unitless
ADI(3,3)	Transformation matrix from I to D-frame	Unitless
ADR(3,3)	Transformation matrix from R to D-frame	Unitless
AGR(3,3)	Transformation matrix from R to G-frame	Unitless
AIB(3,3)	Transformation matrix from B to I-frame	Unitless
AID(3,3)	Transformation matrix from D to I-frame	Unitless
AIG(3,3)	Transformation matrix from G to I-frame	Unitless
ALPHT	Total angle-of-attack	rad
ARB(3,3)	Transformation matrix from B to R-frame	Unitless
ARD(3,3)	Transformation matrix from D to R-frame	Unitless
ARI(3,3)	Transformation matrix from I to R-frame	Unitless
ARP(3,3)	Transformation matrix from P to R-frame	Unitless
ATCOM(45)	Dummy common	Unitless
CA	Axial force coefficient	Unitless
CCCOM(13)	Dummy common	Unitless

<u>Program Symbol</u>	<u>Variable Definition</u>	<u>Units</u>
CH(3)	Coefficients for geodetic latitude computations	Unitless
CEN	Yawing moment coefficient	Unitless
CL	Rolling moment coefficient	Unitless
CLMNT(3)	Aerodynamic moment coefficients about vehicle center of mass	Unitless
CM	Pitching moment coefficient	Unitless
CN	Normal force coefficient	Unitless
CNV	57.29577951	deg/rad
CR	Oblate earth radial coefficient	Unitless
CW	Oblate earth spin axis coefficient	Unitless
CPLMN(3)	Aerodynamic moment coefficient vector about moment reference point	Unitless
CXYZ(3)	Aerodynamic force coefficient vector	Unitless
CY	Side force coefficient	Unitless
DIW(3)	Dummy variable used in gravity gradient torque calculation	slugs-ft ²
DPSI	Difference between geodetic and geocentric latitudes	rad
DREF	Aerodynamic reference diameter	ft
DT	Integration time step	sec
DTP	Output frequency for tape save	sec
DTSAM	Specified time to save variables for restart	sec
EPCOM(66)	Dummy common	Unitless
FAB(3)	B-frame aerodynamic forces	lb
FAI(3)	I-frame aerodynamic forces	lb
FAR(3)	R-frame aerodynamic forces	lb
FARC(3)	R-frame aerodynamic force coefficients	Unitless
FCA(21,11)	Table of axial force coefficients	Unitless
FCEN(21,11)	Table of yawing moment coefficients about moment reference point	Unitless

<u>Program Symbol</u>	<u>Variable Definition</u>	<u>Units</u>
FCL(21,11)	Table of rolling moment coefficients about moment reference point	Unitless
FCM(21,11)	Table of pitching moment coefficients about moment reference point	Unitless
FCN(21,11)	Table of normal force coefficients	Unitless
FCY(21,11)	Table of side force coefficients	Unitless
FOMI(3)	Aerodynamic term in translational acceleration calculation	ft/sec ²
FRHO(11,37)	Table of atmospheric densities	kg/m ³
G(3)	Gravitational acceleration	ft/sec ²
GAMI	Inertial flight path angle (positive up from local geocentric horizontal)	rad
GAMR	Relative flight path angle (positive up from local geodetic horizontal)	rad
GCR	Temporary variable in acceleration of gravity calculation	ft/sec ²
GGB(3)	Gravity gradient torques in B-frame	ft-lb
GMAG	Temporary variable in acceleration of gravity calculation	ft/sec ²
GMASI	Reciprocal of vehicle mass	1/slugs
GMASS	Vehicle mass	slugs
H	Geodetic altitude	ft
HB(3)	Angular momentum in B-frame	ft-lb-sec
IXYZ(3,3)	Moment of inertia tensor	slugs-ft ²
IXYZI(3,3)	Inverse of moment of inertia tensor	1/slugs-ft ²
LAMDA	Inertial longitude measured in I-frame	rad
LAMDE	Earth fixed longitude	rad
LMRP(3)	Temporary variable in aerodynamic moment calculation	Unitless
OMGE	Earth's rotation rate	rad/sec
PCDUM(12)	Dummy common	Unitless
PHIA	Aerodynamic roll angle	rad

<u>Program Symbol</u>	<u>Variable Definition</u>	<u>Units</u>
PHIBK	Bank angle	rad
PI	π	rad
PQR(3)	Angular rates in B-frame	rad/sec
PQRD(3)	Angular accelerations in B-frame	rad/sec ²
PSI	Geocentric latitude (positive north, negative south of equator)	rad
PSID	Geodetic latitude (positive north, negative south of equator)	rad
Q(4)	Quaternion parameters	Unitless
QBAR	Dynamic pressure	lb/ft ²
QD(4)	Time derivatives of quaternions	1/sec
QSQR	$\sqrt{Q(1)^2 + Q(2)^2 + Q(3)^2 + Q(4)^2}$	Unitless
R(3)	Vehicle I-frame position	ft
R1(3)	Unit vector along vehicle I-frame position	Unitless
RB1(3)	Unit vector along vehicle B-frame position	Unitless
RDOT(3)	Vehicle I-frame translational velocity	ft/sec
RHO	Atmospheric density	slugs/ft ³
RMAG	Magnitude of vehicle position vector	ft
RPSI	Radius of the earth	ft
RR,RR2	Temporary variables used in gravitational acceleration calculations	Unitless
SD,SJ,SH	Earth's gravitational constants	Unitless
SIGI	Inertial heading (positive clockwise from north)	rad
SIGR	Relative heading (positive clockwise from north)	rad
SPSI,SPSI2	Temporary variables used in gravitational acceleration calculation	Unitless
SREF	Aerodynamic reference area	ft ²
SWD,SWH	Temporary variables used in gravitational acceleration calculation	Unitless

<u>Program Symbol</u>	<u>Variable Definition</u>	<u>Units</u>
TAB(3)	Total external torques in B-frame	ft-lb
TALP(11)	Table of angle-of-attack values	rad
TEND	Simulation stop time	sec
THOR	Simulation time	hr
TIME	Simulation time	sec
TLAT(11)	Table of geocentric latitude values	rad
TLNG(37)	Table of longitude values	rad
TOA(3)	Aerodynamic torques in B-frame	ft-lb
TPHIA(21)	Table of aerodynamic roll angle values	rad
TRUN	Total run time	sec
TSUM(3)	Time rate of change of vehicle angular momentum	ft lb
TWOPI	2 π	rad
V(3)	Inertial velocity in I-frame	ft/sec
VACOM(67)	Dummy common	Unitless
VATM(3)	Atmospheric velocity in I-frame	ft/sec
VCCOM(18)	Dummy common	Unitless
VDCOM(107)	Dummy common	Unitless
VDOT(3)	Inertial translation acceleration in I-frame	ft/sec ²
VID(3)	Inertial velocity in D-frame	ft/sec
VIG(3)	Inertial velocity in G-frame	ft/sec
VIMAG	Magnitude of inertial velocity	ft/sec
VPCOM(39)	Dummy common	Unitless
VRELB(3)	Relative velocity in B-frame	ft/sec
VRELD(3)	Relative velocity in D-frame	ft/sec
VRELG(3)	Relative velocity in G-frame	ft/sec
VRELI(3)	Relative velocity in I-frame	ft/sec
VRMAG	Magnitude of relative velocity	ft/sec
WT	Vehicle weight	lb
WXH(3)	Angular momentum direction change	ft-lb
XCG,YCG,ZCG	Cg location in N-frame along x,y, and z-axes, respectively	ft

<u>Program Symbol</u>	<u>Variable Definition</u>	<u>Units</u>
XDUM(27)	Dummy common	Unitless
XDDUM(27)	Dummy common	Unitless
XMRP, YMRP, ZMRP	Moment reference point in N-frame along x, y, and z-axes, respectively	ft

Appendix B

REFERENCE FRAMES AND TRANSFORMATIONS

A. Reference Frames

All reference frames are right handed systems (Figs. B-1, B-2, and B-3).

1. I — Inertial Frame. The I-frame has its origin at the center of the earth with the X_I axis through the Greenwich meridian at time zero. The Z_I axis points through the North Pole and the Y_I axis completes the right handed system. It is in this frame the accelerations are integrated.

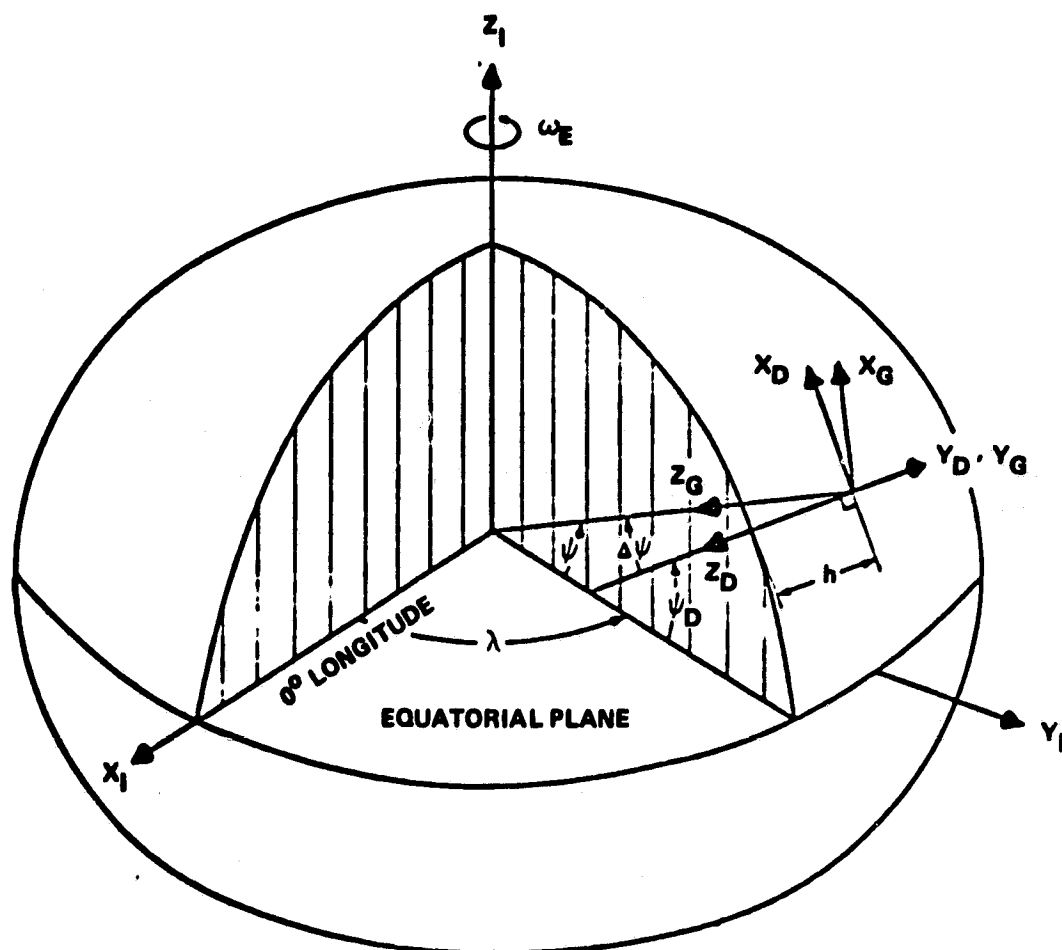
2. G — Geocentric Frame. The G-frame has its origin at the vehicle's center of mass. The X_G axis points north, the Y_G axis points east, and the Z_G axis is directed downward along the radius vector to the earth's center.

3. D — Geodetic Frame. The D-frame has its origin at the vehicle's center of mass (Fig. B-2). The X_D axis points north, the Y_D axis points east, and the Z_D axis is directed downward along the local geodetic.

4. R — Relative Velocity Frame. The R-frame has its origin at the vehicle's center of mass (Fig. B-2). The X_R axis is directed along the relative velocity vector. The Z_R axis is directed downward in a plane containing the velocity vector and the local geodetic. The Y_R axis completes the right handed system.

5. B — Body Frame. The body fixed B-frame has its origin at the vehicle's center of mass (Fig. B-3). The direction of the axes are chosen so as to be consistent with the definition of aerodynamic parameters. It is in this frame that the external forces and moments are computed.

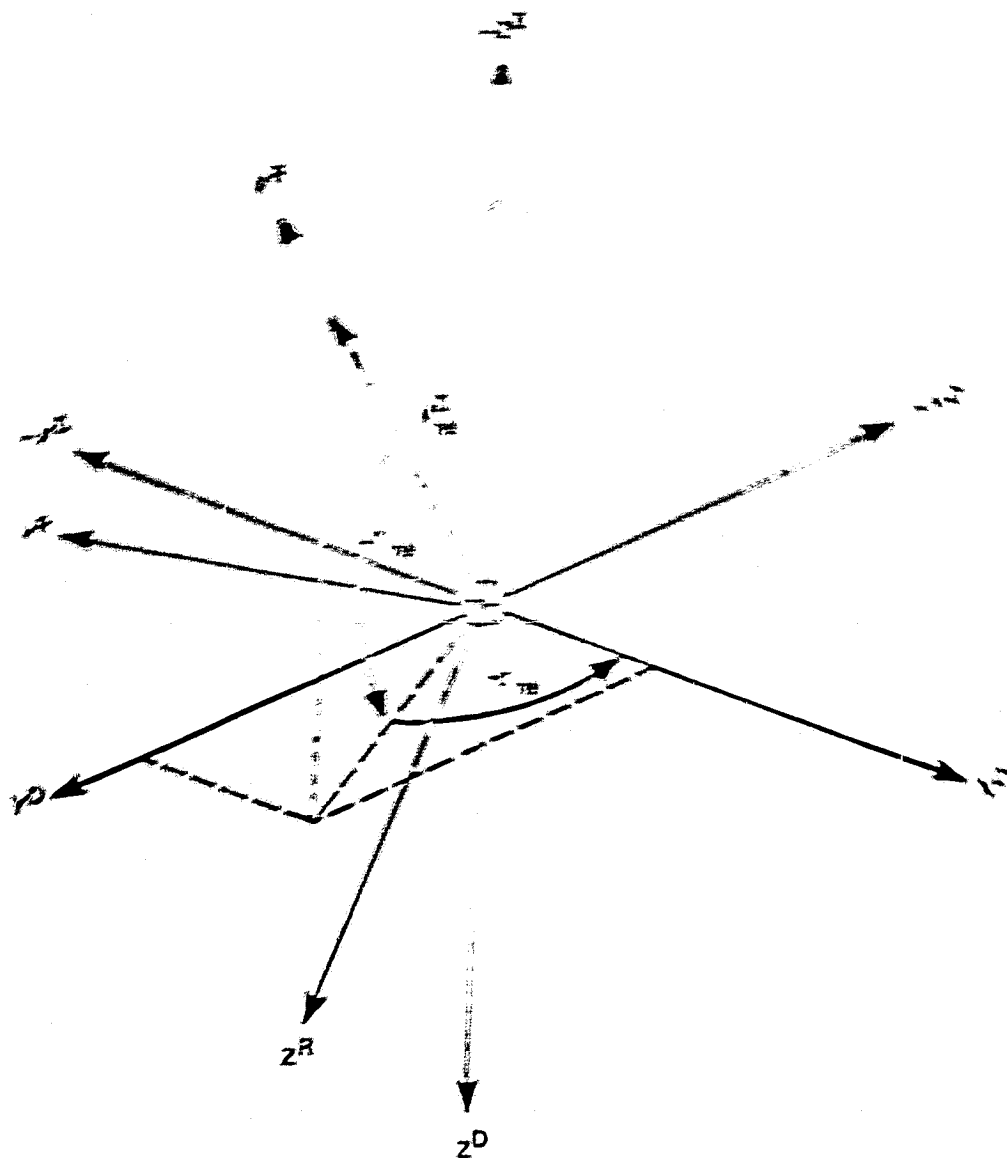
6. N — Input Data Reference Frame. This body fixed reference frame is parallel to the B-frame coordinate system with its origin chosen by the user. It is in this frame that the aerodynamic data and mass properties data are read into the program. Usually, it is convenient to choose the aerodynamic moment reference point as the origin of this frame.



$$A^{GI} = [-(90 + \psi)]_2 [\lambda]_3$$

$$A^{DI} = [-(90 + \psi_D)]_2 [\lambda]_3$$

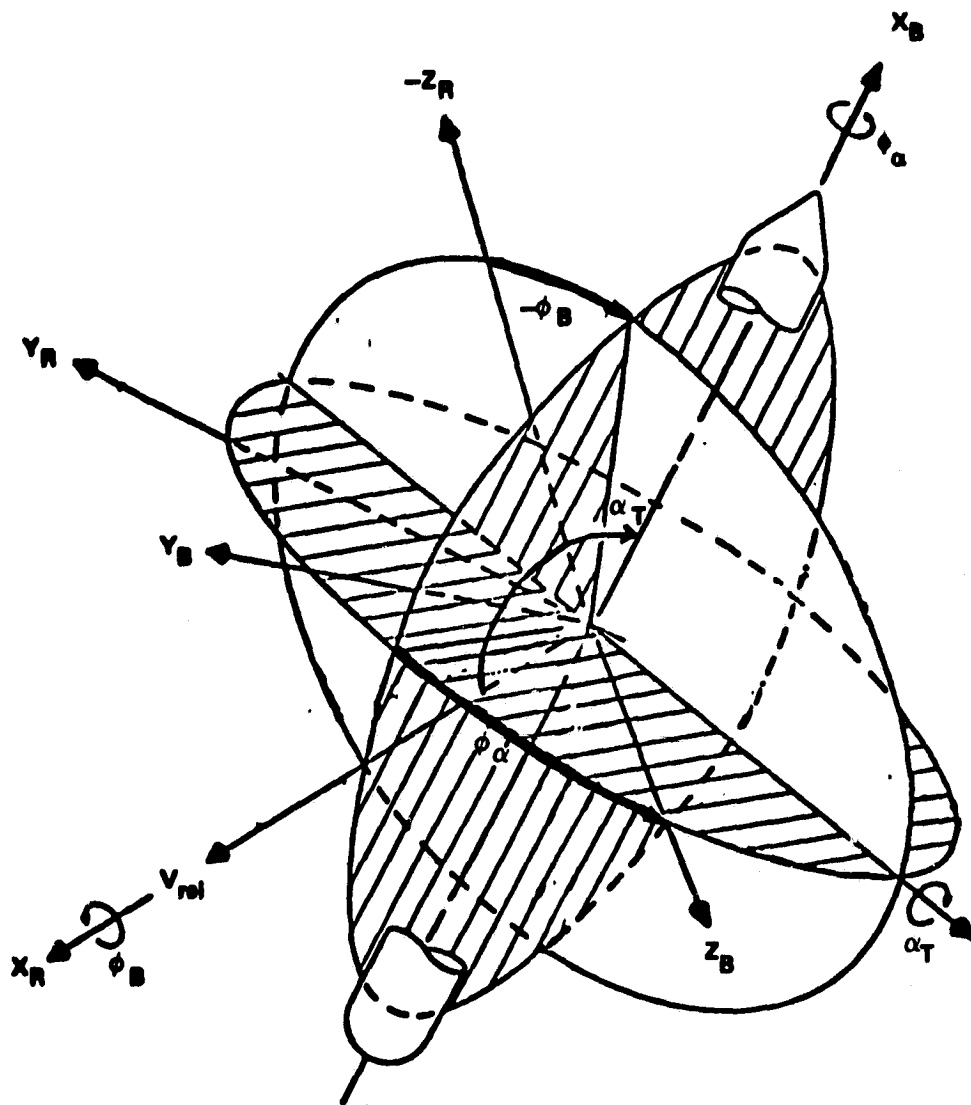
Figure B-1. Inertial (I), geocentric (G) and geodetic (D) reference frames.



$$A^{RD} = [\delta_R]_2 \quad [\sigma_R]_3$$

Figure B-2, Geodetic (D) and relative velocity (R) reference frames.

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$$A^{BR} = [\varphi_\alpha]_1 [\alpha_T]_2 [\varphi_B]_1$$

Figure B-3. Relative velocity (R) and Body (B) reference frames.

B. Transformations

The transformation matrix A^{ML} transforms vectors from the L-frame to the M-frame. The matrices are formed by successive rotations through the indicated Euler angles. The rotation $[\theta]_i$ is used to indicate the direction cosine matrix for a positive rotation about the i^{th} axis through the angle θ . The sequence of rotations is read from right to left. Since all transformations shown are orthogonal, the inverse transformation matrices are merely the transpose of those given.

1. Transformation from I to G-frame A^{GI}

$$A^{GI} = [-(90 + \psi)]_2 [\lambda]_3$$

where λ = inertial longitude

ψ = geocentric latitude

2. Transformation from I to D-frame A^{DI}

$$A^{DI} = [-(90 + \psi_D)]_2 [\lambda]_3$$

where λ = inertial longitude

ψ_D = geodetic latitude

3. Transformation from D to R-frame A^{RD}

$$A^{RD} = [\gamma_R]_2 [\sigma_R]_3$$

where σ_R = relative heading

γ_R = relative flight path angle

4. Transformation from R to B-frame

$$A^{BR} = [\phi_\alpha]_1 [\alpha_T]_2 [\phi_\beta]_1$$

where ϕ_β = bank angle

α_T = total angle-of-attack

ϕ_α = aerodynamic roll angle

5. Transformation from I to B-frame

Initially, the transformation from the I to B-frame is computed by $A^{BI} = A^{BR} A^{RD} A^{DI}$

From the inverse of this transformation, the initial quaternion parameters are computed. The four quaternion parameters are defined as follows:

$$Q_1 = \alpha \sin (\phi / 2)$$

$$Q_2 = \beta \sin (\phi / 2)$$

$$Q_3 = \gamma \sin (\phi / 2)$$

$$Q_4 = \cos (\phi / 2)$$

where α , β , and γ are eigenaxis direction cosines, and ϕ is the eigenaxis rotation angle. The quaternions are initialized as follows:

$$A^{IB} = \begin{bmatrix} a_{11} & a_{12} & a_{13} \\ a_{21} & a_{22} & a_{23} \\ a_{31} & a_{32} & a_{33} \end{bmatrix}$$

$$Q_4 = \frac{1}{2} \sqrt{1 + a_{11} + a_{22} + a_{33}}$$

If $Q_4 \neq 0$,

$$Q_1 = \frac{1}{4 Q_4} (a_{32} - a_{23})$$

$$Q_2 = \frac{1}{4 Q_4} (a_{13} - a_{31})$$

$$Q_3 = \frac{1}{4 Q_4} (a_{21} - a_{12})$$

If $Q_4 = 0$,

$$Q_1 = \sqrt{-\frac{1}{2} (a_{22} + a_{33})}$$

If $Q_1 \neq 0$,

$$Q_2 = \frac{1}{4 Q_1} (a_{12} + a_{21})$$

$$Q_3 = \frac{1}{4 Q_1} (a_{13} + a_{31})$$

If $Q_1 = 0$,

$$Q_2 = \sqrt{\frac{1}{2} (a_{22} + 1)}$$

If $Q_2 \neq 0$,

$$Q_3 = \frac{1}{4 Q_2} (a_{23} + a_{32})$$

If $Q_2 = 0$,

$$Q_3 = 1$$

From the integrated values of the quaternion parameter time derivatives, the A^{IB} transformation matrix is updated as shown in Appendix C.

Appendix C

EQUATIONS OF MOTION

This appendix presents briefly the equations of motion used to describe the dynamics of a vehicle in 6-degrees-of-freedom. The equations were derived for a vehicle of constant mass distribution and the external forces and torques considered were those resulting only from gravity and aerodynamics. The mathematical models for the Earth and gravity can be found in Reference 1. The atmospheric density is an input to the program as a function of position in orbit.

The aerodynamic force and moment coefficients and the atmospheric density are determined by table lookup at each integration step. The aerodynamic coefficients (C_A , C_Y , C_N , C_ℓ , C_m , C_n) are a function of total angle-of-attack, α_T , and aerodynamic roll angle, ϕ_α . The density (ρ) is a function of geocentric latitude, ψ , and inertial longitude, λ . These angles are defined as

$$\alpha_T = \tan^{-1} \frac{\sqrt{V_{REL B}(2)^2 + V_{REL B}(3)^2}}{V_{REL B}(1)} \quad 0 \leq \alpha_T \leq 180^\circ$$

$$\phi_\alpha = \tan^{-1} \frac{V_{REL B}(2)}{V_{REL B}(3)} \quad 0 \leq \phi_\alpha \leq 360^\circ$$

$$\psi = \tan^{-1} \frac{R(3)}{\sqrt{R(1)^2 + R(2)^2}} \quad -90^\circ \leq \psi \leq 90^\circ$$

$$\lambda = \tan^{-1} \frac{R(2)}{R(1)} \quad 0 \leq \lambda \leq 360^\circ$$

where

$\bar{V}_{REL B}$ = relative velocity vector in B-frame

\bar{R} = inertial I-frame position vector.

A. Translational Motion

The translational equation of motion for a body in the inertial I-frame is

$$\ddot{\bar{\mathbf{R}}} = \bar{\mathbf{g}} + \frac{1}{m} \bar{\mathbf{F}}_{AI}$$

where

$$\ddot{\bar{\mathbf{R}}} = \dot{\bar{\mathbf{V}}} = \text{inertial acceleration vector}$$

$$\bar{\mathbf{g}} = \text{gravitational acceleration vector}$$

$$m = \text{mass of the body}$$

$$\bar{\mathbf{F}}_{AI} = \text{I-frame aerodynamic forces}$$

The I-frame velocity equation is

$$\dot{\bar{\mathbf{R}}} = \bar{\mathbf{V}} = \dot{\bar{\mathbf{R}}}_0 + \int \bar{\mathbf{R}} dt$$

where

$$\dot{\bar{\mathbf{R}}}_0 = \bar{\mathbf{V}}_0 = \text{initial I-frame velocity vector.}$$

Integrating the velocity vector and adding the initial position, the I-frame position vector is

$$\bar{\mathbf{R}} = \bar{\mathbf{R}}_0 + \int \dot{\bar{\mathbf{R}}} dt$$

where

$$\bar{\mathbf{R}}_0 = \text{initial I-frame position vector.}$$

The aerodynamic forces are computed in the body B-frame and transformed into the I-frame for the translational acceleration computation. The B-frame aerodynamic forces are

$$\bar{F}_{AB} = q_{BAR} S_{Ref} \bar{C}_{XYZ}$$

where

$$\bar{C}_{XYZ} = \begin{bmatrix} -C_A \\ C_Y \\ -C_N \end{bmatrix} = \text{B-frame aerodynamic force coefficient vector}$$

$$q_{BAR} = \frac{1}{2} \rho |V_{RELB}|^2 = \text{dynamic pressure}$$

$$S_{Ref} = \text{aerodynamic reference area.}$$

Then the I-frame aerodynamic forces are

$$F_{AI} = A^{IB} \bar{F}_{AB} .$$

B. Rotational Motion

The equation describing the rotational motion about the center of mass of a rigid body in the rotating B-frame is given by

$$[I] \dot{\bar{\omega}} = \bar{T}_{AB} - \bar{\omega} \times ([I] \cdot \bar{\omega})$$

where

$$[I] = \begin{bmatrix} I_{XX} & -I_{XY} & -I_{XZ} \\ -I_{XY} & I_{YY} & -I_{YZ} \\ -I_{XZ} & -I_{YZ} & I_{ZZ} \end{bmatrix} = \text{inertia tensor}$$

$\dot{\bar{\omega}} = \overline{PQRD} = \text{B-frame angular acceleration vector}$

$\bar{\omega} = \overline{PQR} = \text{B-frame angular velocity vector}$

$\bar{T}_{AB} = \text{B-frame external torques.}$

Then

$$\bar{\omega} = \bar{\omega}_0 + \int [I]^{-1} [\bar{T}_{AB} - \bar{\omega} \times ([I] \cdot \bar{\omega})] dt$$

where

$\bar{\omega}_0 = \text{initial B-frame angular velocity vector.}$

The aerodynamic torques about the vehicles center of mass are

$$\bar{T}_{OA} = q_{BAR} S_{Ref} D_{Ref} \left[\bar{C}_{PLMN} + \frac{(\bar{X}_{MRP} - \bar{X}_{CG})}{D_{Ref}} \times \bar{C}_{XYZ} \right]$$

where

$D_{Ref} = \text{aerodynamic reference diameter}$

$$\bar{C}_{PLMN} = \begin{bmatrix} C_{\ell} \\ C_m \\ C_n \end{bmatrix} = \text{moment coefficients about the moment reference point}$$

$\bar{X}_{MRP} = \text{aerodynamic moment reference point}$

$\bar{X}_{CG} = \text{center of mass location.}$

The gravitational torques are given by

$$\overline{GGB} = \frac{3 GM}{|R|^3} [\overline{RB1} \times [I] \overline{RB1}]$$

where

GM = product of universal gravitational constant and the mass of the earth

$\overline{RB1}$ = unit vector along body B-frame position.

The B-frame external torques are

$$\overline{T}_{AB} = \overline{T}_{OA} + \overline{GGB} \quad .$$

The quaternion parameters are updated in a similar manner:

$$\overline{Q} = \overline{Q}_0 + \int \dot{\overline{Q}} dt$$

where

\overline{Q}_0 = initial quaternion parameters defined in Appendix B.

The time derivivity $\dot{\overline{Q}}$ is defined as

$$\dot{\overline{Q}} = \begin{bmatrix} \dot{Q}_1 \\ \dot{Q}_2 \\ \dot{Q}_3 \\ \dot{Q}_4 \end{bmatrix} = \begin{bmatrix} Q_4 & -Q_3 & Q_2 \\ Q_3 & Q_4 & -Q_1 \\ -Q_2 & Q_1 & -Q_4 \\ -Q_1 & -Q_2 & -Q_3 \end{bmatrix} \overline{\omega} \quad .$$

From these integrated values of \bar{Q} , the A^{IB} transformation matrix is calculated as follows:

$$A^{IB} = \begin{bmatrix} (2 Q_1^2 + 2 Q_4^2 - 1) & 2(Q_1 Q_2 - Q_3 Q_4) & 2(Q_1 Q_3 + Q_2 Q_4) \\ 2(Q_1 Q_2 + Q_3 Q_4) & (2 Q_2^2 + 2 Q_4^2 - 1) & 2(Q_2 Q_3 - Q_1 Q_4) \\ 2(Q_1 Q_3 - Q_2 Q_4) & 2(Q_2 Q_3 + Q_1 Q_4) & (2 Q_3^2 + 2 Q_4^2 - 1) \end{bmatrix}$$

Appendix D

PROGRAM LISTING

```

1. SKYLAB DYNAMICS PROGRAM(SKYDYN)
2.
3.
4.
5.
6.
7. THIS PROGRAM IS AN ALTERED VERSION OF NORTHROP SERVICES PROGRAM
8. REENTR - SPACE SHUTTLE EXTERNAL TANK REENTRY SIMULATION. THE
9. THEORY USED IN THIS PROGRAM IS DOCUMENTED IN -
10. M-250-1303
11. MANY OF THE OPTIONS IN PROGRAM REENTR ARE DELETED IN
12. ORDER TO GIVE MAXIMUM SPEED TO THIS VERSION.
13.
14. ASSUMPTIONS
15.
16. 1. FISCHER ELLIPSOID EARTH MODEL
17. 2. DENSITY INPUT AS FUNCTION OF ORBITAL POSITION ONLY
18. 3. AERO COEFFICIENTS DEPENDENT ONLY OF ATTITUDE
19. 4. CONSTANT MASS DISTRIBUTION
20. 5. ASRU AND GRAVITY TOLERANCES
21.
22.
23.
24. REAL INVTZ(3,3),INVTZ(3,3),LMRP(3),LANDA,LANDOE
25. REAL INVTX(3,3),LMRPX(3),LKC(3)
26. DIMENSION IVAR(90),SCALE(90),PVALU(90),PNAME(90),CASE(18),
27. SAI(3,3),A(3,3),A(3),A(3),A(3,3),IPN(90),PLT(90)
28. DIMENSION ATNH(13),LI(3),MI(3),ABP(3,3)
29.
30.
31.
32.
33. PROGRAM CONTROL AND INTEGRATION (100)
34.
35. COMMON TIME,DT,DTF,DTSAM,TRUM,TEND,THOR,QSCR,PCOUN(12)
36. COMMON PQRD(3),QD(4),VDDI(3),ADDT(3),XDDUN(27)
37. COMMON PQR(3),G(4),V(3),R(3),XOUN(27)
38.
39. VEHICLE CHARACTERISTICS COMMON (50)
40.
41. COMMON WT,XCG,YCG,ZCG,INVTZ,INVTZ,OREF,SREF,LMRP,CMASS,CHAST,
42. $ XMRP,YMRP,ZMRP,VCCUN(18)
43.
44. VEHICLE POSITION COMMON (150)
45.
46. COMMON PHURK,ALPHU,PHI,ARB(3,3),AIB(3,3),ARP(3,3),ABI(3,3),
47. $ AID(3,3),AIG(3,3),AGR(3,3),ADR(3,3),ADI(3,3),ADS(3,3),
48. $ AND(3,3),ARI(3,3),VPCON(39)
49.
50. EARTH POSITION COMMON (100)
51.
52. COMMON RMAG,RPST,RI(3),G(3),CR,CV,CMAG,RR,RR2,SPSI,SPSI2,SJ,

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53. \$ SD,SH,SMH,SHD,GCR,H,PSI,DPSI,PSID,LANDA,LANDE,SICR,CAMR,
54. \$ SIGI,CAMI,RBL(3),EPCOM(66)
55. C
56. C VEHICLE AERODYNAMICS COMMON (100)
57. C
58. COMMON CA,CH,CL,CM,CT,CEM,FAR(3),PARC(3),CPLMH(3),CHYZ(3),
59. \$ CLMNT(3),FAR(3),FAI(3),FOMI(3),TOA(3),VACOM(67)
60. C
61. C
62. C VEHICLE DYNAMICS COMMON (150)
63. C
64. COMMON RHO,QBAR,VRMAG,VRELD(3),VINAG,VID(3),VRELC(3),
65. \$ VRELI(3),VRELB(3),VATM(3),DIM(3),GCB(3),VIC(3),TAB(3),
66. \$ HB(3),WXH(3),TSUM(3),VDCOM(107)
67. C
68. C THE FOLLOWING VARIABLES ARE NOT CHANGED FROM CASE TO CASE AND
69. C ARE CONSIDERED AS CONSTANTS
70. C
71. C ATMOSPHERE TABLES COMMON (500)
72. C
73. C
74. COMMON TLA(11),TLNC(37),ERHO(11,37),ATCOM(45)
75. C
76. C TABLES OF AERODYNAMIC COEFFICIENTS COMMON (2000)
77. C
78. COMMON TALP(11),TPHIA(21),FCM(21,11),FCA(21,11),
79. \$ FCY(21,11),FCL(21,11),FCM(21,11),FCEN(21,11),ACCOM(582)
80. C
81. C
82. C
83. C CHANGELESS CONSTANTS COMMON(20)
84. C
85. COMMON CH(3),TWOPI,OMGE,CNV,PI,CCCOM(13)
86. C
87. C
88. C TOTAL POINTS IN COMMON BLOCK = 3170
89. C TOTAL POINTS IN VARYING COMMON = 650
90. C
91. C
92. C DATA BLANK/4H /
93. C
94. C NCASE = NO. OF CASES TO BE RUN PER CASE DECK
95. C
96. C NX = NO. OF INTEGRATION VARIABLES
97. C
98. C
99. CALL EBOMB(94S)
100. READ(5,1)NCASE,NX
101. 1 FORMAT(3I5)
102. NR = 5
103. NW = 6
104. NP = 12

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105. NCOM = 656
106. NCOM1 = 3170
107. C*****ZERO COMPLETE COMMON BLOCK
108. CALL ZCOM(NCOM1)
109. C*****READ MAIN PRINT SPECIFICATIONS
110. CALL PSPEC(5,6,12,NPV,IVAR,PHAME,SCALE,IPM)
111. C*****READ IN ATMOSPHERIC DATA
112. 4 FORMAT(2F10.5,15)
113. READ(5,5)(ATNM(I),I=1,18)
114. 5 FORMAT(18A4)
115. READ(5,300)(TLAT(I),I=1,11)
116. READ(5,300)(TLNG(I),I=1,37)
117. 00 337 J=1,37
118. 337 READ(5,6)(FRHO(I,J),I=1,11)
119. 6 FORMAT(6E9.3)
120. CNV = 57.29577951
121. C*****READ IN VEHICLE AERODYNAMIC DATA
122. READ(NR,301)NALP,NPHIA
123. 301 FORMAT(5I5)
124. C
125. C*****READ IN ALPHAT AND PHIA INDEPENDENT VARIABLE TABLES
126. C
127. 302 FORMAT(9F8.3)
128. READ(NR,300)(TALP(I),I=1,NALP)
129. READ(NR,300)(TPHIA(I),I=1,NPHIA)
130. 303 FORMAT(6E12.1)
131. C
132. C***AXIAL FORCE COEFFICIENT TABLE
133. C
134. 300 FORMAT(2E8.3)
135. READ(NR,300)((FCA(I,J),I=1,NPHIA),J=1,NALP)
136. C
137. C***NORMAL FORCE COEFFICIENT TABLE
138. C
139. READ(NR,300)((FCN(I,J),I=1,NPHIA),J=1,NALP)
140. C
141. C***SIDE FORCE COEFFICIENT TABLE
142. C
143. READ(NR,300)((FCY(I,J),I=1,NPHIA),J=1,NALP)
144. C
145. C***PITCHING MOMENT COEFFICIENT TABLE
146. C
147. READ(NR,300)((FCM(I,J),I=1,NPHIA),J=1,NALP)
148. C
149. C***YAWING MOMENT COEFFICIENT TABLE
150. C
151. READ(NR,300)((FCEN(I,J),I=1,NPHIA),J=1,NALP)
152. C
153. C***ROLLING MOMENT COEFFICIENT TABLE
154. C
155. READ(NR,300)((FCL(I,J),I=1,NPHIA),J=1,NALP)
156. C

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157. C
158. 00 334-I=1,NALP
159. 334 TALP(I)=TALP(I)/CNV
160. 00 335-I=1,NPHIA
161. 335 TPHIA(I)=TPHIA(I)/CNV
162. 00 338-I=1,11
163. 338 TLAT(I)=TLAT(I)/CNV
164. 00 339-I=1,37
165. 339 TLANG(I)=TLANG(I)/CNV
166. PI=180-/CNV
167. TWOPI=2.*PI
168. CM=1.40765391E16
169. RE=20925721.785
170. RS=20909734.843
171. GF=0.6738525415E-02
172. GJ=-.162405E-02
173. GH=-.640E-05
174. GD=-.69125E-05
175. OMGE=7.29221158E-05
176. CH0=3.3718120539E-03
177. CH(1)=-1.57258544E-10
178. CH(2)=5.907450825E-18
179. CH(3)=-1.08416187E-25
180. 7 FORMAT(8E10.1)
181. ICASE=0
182. C****BEGIN CASE LOOP
183. 8 CALL ZCOM(NCOM)
184. ICASE=ICASE+1
185. IF(ICASE.GT.1)GO TO 11
186. C
187. C****READ CASE DEFINITION DATA
188. C
189. C
190. C
191. READ(5,5)(CASE(I),I=1,18)
192. IF(CASE(1).EQ.BLANK)GO TO 94
193. READ(5,2)PROPT
194. READ(5, 2)DT,DTP,DTSAM,TRUN,TIME,IOP1
195. 2 FORMAT(5F10.4,I5)
196. DTX=DT
197. DTPX=DTP
198. DTSX=DTSAM
199. TRUNX=TRUN
200. TIMEX=TIME
201. GO TO 12
202. 11 IF(ICASE.GT.NCASE)GO TO 90
203. DT=DTX
204. DTP=DTPX
205. DTSAM=DTSX
206. TRUN=TRUNX
207. TIME=TIMEX
208. C

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209. C****INITIALIZE VARIABLES
210. C
211. 12 TEND=TRUN+TIME
212. TP=TIME
213. TPD=TIME
214. IF(ICASE.CT.1).GO TO 17
215. C****READ VEHICLE DATA
216. READ(5,13)WT,XCG,YCG,ZCG,XMRP,YMRP,ZMRP
217. 13 FORMAT(8F10.4)
218. READ(5,13)DREF,SREF
219. READ(5,7)XYZ(1,1),XYZ(2,2),XYZ(3,3),XYZ(1,2),XYZ(1,3),
220. XYZ(2,3)
221. XYZ(1,2)=-XYZ(1,2)
222. XYZ(1,3)=-XYZ(1,3)
223. XYZ(2,3)=-XYZ(2,3)
224. XYZ(2,1)=XYZ(1,2)
225. XYZ(3,1)=XYZ(1,3)
226. XYZ(3,2)=XYZ(2,3)
227. LMRP(1)=(XMRP-XCG)/DREF
228. LMRP(2)=(YMRP-YCG)/DREF
229. LMRP(3)=(ZMRP-ZCG)/DREF
230. WTX=WT
231. DREFX=DREF
232. SREFX=SREF
233. DO 14 I=1,3
234. DO 14 J=1,3
235. XYZX(I,J)=XYZ(I,J)
236. LMRPX(I)=LMRP(I)
237. 14 CONTINUE
238. C
239. C****POSITION INITIALIZATION
240. C
241. READ(5,15)PSI,LANDE,RNAG,VINAG,SIGI,GAMI
242. LANDA=LANDE+OMGE*TIME*CNV
243. 15 FORMAT(F10.6,F10.5,F10.2,F10.3,F10.6,F10.8)
244. READ(5,16)PHIBI,ALPHAI,PHIAI,(PQR(I),I=1,3)
245. READ(5,210)((ABP(I,J),J=1,3),I=1,3)
246. 16 FORMAT(6F10.5)
247. PSIX=PSI
248. XLAND=LANDE
249. RNAGX=RNAG
250. VRELX=VINAG
251. SIGIX=SIGI
252. GAMIX=GAMI
253. PHIAIX=PHIAI
254. ALPAIX=ALPHAI
255. PHIBIX=PHIBI
256. PP=PQR(1)
257. PQ=PQR(2)
258. PR=PQR(3)
259. GO TO 19
260. 17 CONTINUE

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261. WT=WTX
262. DREF=DREFX
263. SREF=SREFX
264. DO 18 I=1,3
265. DO 18 J=1,3
266. IXYZ(I,J)=IXYZ(I,J)
267. LMRP(I)=LMRPX(I)
268. 18 CONTINUE
269. PSI=PSIX
270. LAMDA=XLAMDA*ONCE*TIMEX*CNV
271. RMAG=RMAGX
272. VMAG=VR6LX
273. SIGI=SIGIX
274. GAMI=GAMIX
275. PHIAT=PHIATX
276. ALPHAT=ALPHATX
277. PHIBI=PHIBIX
278. PQR(1)=PP
279. PQR(2)=PQ
280. PQR(3)=PR
281. 19 CONTINUE
282. LAMDA=LAMDA/CNV
283. LAMDE=LAMDE/CNV
284. PSI=PSI/CNV
285. SIGI=SIGI/CNV
286. GAMI=GAMI/CNV
287. PHIAT=PHIAT/CNV
288. ALPHAT=ALPHAT/CNV
289. PHIBI=PHIBI/CNV
290. DO 20 I=1,3
291. PQR(I)=PQR(I)/CNV
292. GHAS=WT*RS*RS/GM
293. GHASI=1./GHAS
294. DO 21 I=1,3
295. DO 21 J=1,3
296. 21 IXYZ(I,J)=IXYZ(I,J)
297. CALL MINV(IXYZ1,3,DI,LI,MI)
298. C
299. C
300. C
301. INERTIAL POSITION VECTOR COMPUTATION
302. RPSI=RE/SQRT(1.+GF*(SIN(PSI)**2))
303. H=RMAG-RPSI
304. R(1)=RMAG*COS(PSI)*COS(LAMDA)
305. R(2)=RMAG*COS(PSI)*SIN(LAMDA)
306. R(3)=RMAG*SIN(PSI)
307. DPSI=CHO
308. HW=1.
309. DO 22 I=1,3
310. HW=HW*H
311. DPSI=DPSI+CH(I)*HW
312. PSID=DPSI*PSI+DPSI

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313. C
314. C***GEOCENTRIC COMPUTATIONS
315. C
316. CALL TWIST(LAMDA,A1,3)
317. PS19=PS10+90./CNV
318. CALL TWIST(-PS19,A2,2)
319. DO 23 I=1,3
320. DO 23 J=1,3
321. 23 AID(I,J)=A1(I,1)*A2(I,J)+A1(I,2)*A2(2,J)+A1(I,3)*A2(3,J)
322. C
323. C***GEOCENTRIC COMPUTATIONS
324. C
325. PS90=PS1+90./CNV
326. CALL TWIST(-PS90,A2,2)
327. DO 24 I=1,3
328. DO 24 J=1,3
329. 24 AIG(I,J)=A1(I,1)*A2(I,J)+A1(I,2)*A2(2,J)+A1(I,3)*A2(3,J)
330. DO 350 I=1,3
331. DO 350 J=1,3
332. 350 ADI(I,J)=AID(J,I)
333. C
334. C D-FRAME INERTIAL VELOCITY COMPONENTS
335. C
336. VIG(1)=VINAG*COS(GAMI)*COS(SIGI)
337. VIG(2)=VINAG*COS(GAMI)*SIN(SIGI)
338. VIG(3)=VINAG*SIN(GAMI)
339. CALL TWIST(DPSI,ADG,2)
340. DO 25 I=1,3
341. 25 VID(I)=ADG(I,1)*VIG(1)+ADG(I,2)*VIG(2)+ADG(I,3)*VIG(3)
342. C
343. C COMPUTE INITIAL ATMOSPHERIC VELOCITY COMPONENTS(INERTIAL FRAME)
344. C
345. VATM(1)=OMGE*R(2)
346. VATM(2)=OMGE*R(1)
347. VATM(3)=0.0
349. C
350. C RESOLVE VECTORS INTO I-FRAME
351. C
352. DO 29 I=1,3
353. V(I)=AID(I,1)*VID(1)+AID(I,2)*VID(2)+AID(I,3)*VID(3)
354. 29 A(I)=V(I)-VATM(I)
355. C D-FRAME RELATIVE VELOCITY COMPONENTS
356. DO 351 I=1,3
357. 351 VREL(I)=ADI(I,1)*A(I,1)+ADI(I,2)*A(2)+ADI(I,3)*A(3)
359. C
360. C DETERMINE EULER MATRIX FROM RELATIVE VELOCITY FRAM TO BODY FRAME
361. CALL TWIST(-ALPHA,A1,2)
362. CALL TWIST(-PHI1,A2,1)
363. DO 30 I=1,3
364. DO 30 J=1,3
365. 30 A3(I,J)=A1(I,1)*A2(I,J)+A1(I,2)*A2(2,J)+A1(I,3)*A2(3,J)

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417. $,11HLONGITUDE =,F10.5/1X,19HINERTIAL VELOCITY =,F10.3/1X,10HINERTI
418. $AL HEADING =,F10.5/1X,28HINERTIAL FLIGHT PATH ANGLE =,F10.6/1X,23
419. $HVEHICLE ATTITUDE DATA =,1X,11HPHIDI +1 =,F10.5/
420. $ 25X,11H LPHAI +2 =,F10.5/25X,11HPHAI +1 =,F10.5/1X,
421. $18HINITIAL BODY RATES,
422. $6X,11HROLL RATE =,F10.5/25X,12HPITCH RATE =,F10.5/25X,10HYAW RATE
423. $ =,F10.5/1X
424. WRITE(6,41)
425. WRITE(6,46)
426.
427. 46 FORMAT(1X,32H*****OTHER INFORMATION*****/)
428. WRITE(6,47)(ATNM(I),I=1,18)
429. 47 FORMAT(1X,20HTHIS PROGRAM USES ,10A4/)
430. WRITE(6,98)DT,DTP,DTSM,TRUN,TINE,IOP1
431. 98 FORMAT(1X,4HDELT,F10.6,5X,4HDTSM,F10.5,5X,4HDTPR,F10.5,5X,4HDTSM,F10.2,5X,
432. 14HTRUN,F10.2,5X,4HTIME,F10.2,4X,5HIOP1,13)
433. 210 FORMAT(6E12.6/3E12.6)
434. 211 FORMAT(1X,4HARP ,5X,3E18.7/10X,3E18.7/10X,3E18.7/)
435. C
436. IF(IOP1.EQ.0) GO TO 600
437. READ(14)(TIME,DT,(PORD(I),PDR(I),VDDOT(I),V(I),
438. $RDOT(I),R(I),I=1,3),QD(J),Q(J),J=1,4))
439. 600 CONTINUE
440. C*****BEGIN INTEGRATION LOOP
441. 51 CONTINUE
442. DO 86 KUTTA=1,5
443. C
444. C*****EVALUATE DERIVATIVES
445. C
446. RMAG=SQRT(R(1)*R(1)+R(2)*R(2)+R(3)*R(3))
447. R1(1)=R(1)/RMAG
448. R1(2)=R(2)/RMAG
449. R1(3)=R(3)/RMAG
450. GMAG=GM/(RMAG*RMAG)
451. RR=RE/RMAG
452. RR2=RR*RR
453. SPSI=RI(3)
454. SPSI2=SPSI*SPSI
455. RPSI=RE/SQRT(1.+GF*SPSI2)
456. SJ=1.-5.*SPSI2
457. SD=1./7.-2.*SPSI2+3.*SPSI2*SPSI2
458. SH=3.-7.*SPSI2
459. SMH=SJ/5
460. SMD=SH/7
461. CR=RR2*(GH*RR*SPSI*SH+3.*GD*RR2*SD+CJ*SJ)+1.
462. CM=RR2*(3.*GH*RR*SMH+4.*GD*RR2*SPSI*SMD+2.*CJ*SPSI)
463. GCR=GMAG*CR
464. G(1)=GCR*RI(1)
465. G(2)=GCR*RI(2)
466. G(3)=GMAG*CM+GCR*RI(3)
467. H=RMAG-RPSI
468. PSI=ATN2(R(3),SQRT(R(1)*R(1)+R(2)*R(2)))
N=3

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469.      DPSI=CHQ
470.      HW=1.
471.      DO 53 I=1,N
472.      HW=HW*H
473.      53 DPSI=DPSI+CH(I)*HW
474.      DPSI=DPSI*SIN(2.0*PSI)
475.      PSIO=DPSI+DPSI
476.      PSI90=PSIO+90./CNV
477.      LAMDA=ATN2(R(2),R(1))
478.      CALL TWIST(LAMDA,A3,3)
479.      CALL TWIST(-PSI90,A2,2)
480.      DO 54 J=1,3
481.      DO 54 J=1,3
482.      54 AID(I,J)=A3(I,1)*A2(I,1)*A3(I,2)*A2(2,J)*A3(I,3)*A2(3,J)
483.      PSG90=PSI+90./CNV
484.      CALL TWIST(-PSG90,A2,2)
485.      DO 58 I=1,3
486.      DO 58 J=1,3
487.      58 AIG(I,J)=A3(I,1)*A2(I,1)*A3(I,2)*A2(2,J)*A3(I,3)*A2(3,J)
488.      VATM(1)=-OMGE*R(2)
489.      VATM(2)=OMGE*R(1)
490.      VATM(3)=0.0
491.      DO 55 I=1,3
492.      55 VRELI(I)=V(I)-VATM(I)
493.      VRMAG=SQRT(VRELI(1)*VRELI(1)+VRELI(2)*VRELI(2)+VRELI(3)*VRELI(3))
494.      CALL SULR5(Q,AIB)
495.      DO 56 I=1,3
496.      DO 56 J=1,3
497.      56 ABI(I,J)=AIB(J,I)
498.      DO 57 I=1,3
499.      R81(I)=-ABI(I,1)*R1(1)-ABI(I,2)*R1(2)-ABI(I,3)*R1(3)
500.      57 VRELB(I)=ABI(I,1)*VRELI(1)+ABI(I,2)*VRELI(2)+ABI(I,3)*VRELI(3)
501.      C*****
502.      C
503.      C AERODYNAMIC FORCES AND MOMENTS
504.      C
505.      C*****
506.      C
507.      IF(LAMDA.LT.0.) LAMDA=LAMDA+TWOP1
508.      CALL LOOK2(RHO,FRHO,11,PSI,TLAT,11,LAMDA,TLNG,37,IPSI,ILNG,
509.      $ 1)
510.      RHO=RHO*1.9349971E-03
511.      QBAR=0.5*RHO*VRMAG*VRMAG
512.      ALPHT=ATN2(SQRT(VRELB(2)*VRELB(2)+VRELB(3)*VRELB(3)),VRELB(1))
513.      PHIA=ATN2(VRELB(2),VRELB(3))
514.      IF(PHIA.LT.0.6)PHIA=PHIA+TWOP1
515.      501 CONTINUE
516.      C
517.      C*****MAIN BODY COEFFICIENTS
518.      C
519.      C
520.      CALL LOOK2(CN,FCN,21,PHIA,TPHIA,NPHIA,ALPHT,TALP,NALP,IPHIA,IALP,

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521. S 1)
522. CALL LOOK2 CA,FCA,21,PHIA,TPHIA,NPHIA,ALPHT,TALP,NALP,IPHIA,IALP,
523. S 0)
524. CALL LOOK2(CM,FCM,21,PHIA,TPHIA,NPHIA,ALPHT,TALP,NALP,IPHIA,IALP,
525. S 0)
526. CALL LOOK2(CV,FCV,21,PHIA,TPHIA,NPHIA,ALPHT,TALP,NALP,IPHIA,IALP,
527. S 0)
528. CALL LOOK2(CL,FCL,21,PHIA,TPHIA,NPHIA,ALPHT,TALP,NALP,IPHIA,IALP,
529. S 0)
530. CALL LOOK2(CCM,FCCM,21,PHIA,TPHIA,NPHIA,ALPHT,TALP,NALP,IPHIA,IALP,
531. S 0)
532. CPLMN(1)=CL
533. CPLMN(2)=CM
534. CPLMN(3)=CEN
535. XYZ(1)=-CA
536. XYZ(2)=CV
537. XYZ(3)=-CN
538. LXC(1)=LMRP(2)*XYZ(3)-LMRP(3)*XYZ(2)
539. LXC(2)=LMRP(3)*XYZ(1)-LMRP(1)*XYZ(3)
540. LXC(3)=LMRP(1)*XYZ(2)-LMRP(2)*XYZ(1)
541. DO 63 I=1,3
542. DIM(1)=XYZ(1,1)*RBI(1)+XYZ(1,2)*RBI(2)+XYZ(1,3)*RBI(3)
543. 63 CLMNT(1)=CPLMN(1)*LXC(1)
544. GGB(1)=RBI(2)*DIM(3)-RBI(3)*DIM(2)
545. GGB(2)=RBI(3)*DIM(1)-RBI(1)*DIM(3)
546. GGB(3)=RBI(1)*DIM(2)-RBI(2)*DIM(1)
547. GGB(1)=GGB(1)*(CM*3.0/RMAG**2)/RMAG
548. GGB(2)=GGB(2)*(CM*3.0/RMAG**2)/RMAG
549. GGB(3)=GGB(3)*(CM*3.0/RMAG**2)/RMAG
550. QS=QBAR*SREF
551. QSD=QS*DREF
552. DO 64 I=1,3
553. FAB(I)=XYZ(1)*QS
554. TOA(I)=CLMNT(1)*QSD
555. 64 TAB(I)=TOA(I)+GGB(I)
556. C*****
557. C
558. C RIGID BODY DYNAMICS
559. C
560. C*****
561. DO 65 I=1,3
562. 65 HB(I)=XYZ(1,1)*PQR(1)+XYZ(1,2)*PQR(2)+XYZ(1,3)*PQR(3)
563. WXH(1)=PQR(2)*HB(3)-PQR(3)*HB(2)
564. WXH(2)=PQR(3)*HB(1)-PQR(1)*HB(3)
565. WXH(3)=PQR(1)*HB(2)-PQR(2)*HB(1)
566. DO 66 I=1,3
567. 66 TSUM(I)=TAB(I)-WXH(I)
568. DO 67 I=1,3
569. 67 PQRD(I)=XYZ(1,1)*TSUM(1)+XYZ(1,2)*TSUM(2)+XYZ(1,3)*TSUM(3)
570. QD(1)=.5*(Q(4)*PQR(1)-Q(3)*PQR(2)+Q(2)*PQR(3))
571. QD(2)=.5*(Q(3)*PQR(1)+Q(4)*PQR(2)-Q(1)*PQR(3))
572. QD(3)=.5*(-Q(2)*PQR(1)+Q(1)*PQR(2)+Q(4)*PQR(3))

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573. Q0(4)=-.5*(Q(1)*PQR(1)+Q(2)*PQR(2)+Q(3)*PQR(3))
574. QSOR=SQRT(Q(1)*.2+Q(2)*.2+Q(3)*.2+Q(4)*.2)
575. DO 68 I=1,3
576. FAL(I)=AIB(I,1)*FAB(1,2)+AIB(I,2)*FAB(2,3)+AIB(I,3)*FAB(3,4)
577. FOMI(I)=FAL(I)*GNASI
578. YDOT(I)=FOMI(I)+G(I)
579. 68 ROOT(I)=V(I)
580. IF(KUTTA-I) 86,69,86
581. C
582. C*****PERFORM END-OF-DISTEP COMPUTATIONS
583. 69 CONTINUE
584. C
585. LAMDE=ATN2(R(2),R(1))-ONCE*TIME
586. 497 IF(LAMDE)498,499,499
587. 498 LAMDE=LAMDE+TWOP
588. GO TO 497
589. 499 CONTINUE
590. DO 101 I=1,3
591. DO 101 J=1,3
592. 101 ADI(I,J)=AID(J,I)
593. DO 103 I=1,3
594. VIG(I)=AIG(I,1)*V(1)+AIG(I,2)*V(2)+AIG(I,3)*V(3)
595. VID(I)=ADI(I,1)*V(1)+ADI(I,2)*V(2)+ADI(I,3)*V(3)
596. VINAG=SQRT(V(1)*V(1)+V(2)*V(2)+V(3)*V(3))
597. DO 102 I=1,3
598. 102 VREL(I)=ADI(I,1)*VREL(1)+ADI(I,2)*VREL(2)+ADI(I,3)*VREL(3)
599. GAMR=ATN2(-VREL(3),SQRT(VREL(1)*VREL(1)+VREL(2)*VREL(2)))
600. SIGR=ATN2(VREL(2),VREL(1))
601. GANI=ATN2(-VIG(3),SQRT(VIG(1)*VIG(1)+VIG(2)*VIG(2)))
602. SIGI=ATN2(VIG(2),VIG(1))
603. CALL TWISTESIGR,AL,3
604. CALL TWISTESIGR,A2,2
605. DO 104 I=1,3
606. DO 104 J=1,3
607. 104 ADR(I,J)=A1(I,1)*A2(I,2)+A1(I,3)*A2(2,3)+A1(I,3)*A2(3,3)
608. DO 105 I=1,3
609. DO 105 J=1,3
610. 105 ARD(I,J)=ADR(J,I)
611. DO 106 I=1,3
612. DO 106 J=1,3
613. 106 ARI(I,J)=ARD(I,1)*ARI(I,2)+ARD(I,2)*ARI(2,3)+ARD(I,3)*ARI(3,3)
614. DO 107 I=1,3
615. DO 107 J=1,3
616. 107 ARB(I,J)=ARI(I,1)*ARB(I,2)+ARI(I,2)*ARB(2,3)+ARI(I,3)*ARB(3,3)
617. DO 212 I=1,3
618. DO 212 J=1,3
619. 212 ARP(I,J)=ARB(I,1)*ARP(I,2)+ARB(I,2)*ARP(2,3)+ARB(I,3)*ARP(3,3)
620. PHIBK=ATN2(ARB(2,1),-ARB(3,1))
621. DO 110 I=1,3
622. FAR(I)=ARD(I,1)*FAB(1,2)+ARB(1,2)*FAB(2,3)+ARB(1,3)*FAB(3,4)
623. 110 FARC(I)=FAR(I)/QS
624. C

```

```

625. C*****PRINT IF APPROPRIATE
626. C
627. IF(TIME-TP)74,73,73
628. C
629. 73 CONTINUE
630.  TWDZ=TIME/3600.0
631.  NXPR=1
632.  IF(TIME-TPR)120,121,121
633.  120 NXPR=-1
634.  121 CONTINUE
635.  IF(TIME.LT.DTSAM) GO TO 601
636.  WRITE(13)(TIME,DT,(PQR(I),PQR(I),VDT(I),V(I),
637.  $RDT(I),P(I),I=1,3),(QD(J),Q(J),J=1,4))
638.  DTSAM=DTSAM+TEND
639.  NXPR=1
640.  601 CONTINUE
641.  IF(NXPR.GT.0)TPR=TIME+PROPT*DTP
642.  IF(TIME.GE.TEND)NXPR=1
643.  CALL BLOCK( 6,NP,CASE,NPV,IVAR,PHASE,PVALD,SCALE,IPU,NIPR)
644.  TP=TIME+DTP
645.  C
646. C*****CHECK WHETHER THIS CASE SHOULD BE TERMINATED
647. C
648. 74 CONTINUE
649.  IF(TIME-TEND)86,87,87
650. C
651. C*****INTEGRATE DYNAMIC VARIABLES
652. C
653. 86 CALL RUNK2(KUTTA,MX)
654.  GO TO 51
655. C
656. C*****TERMINATE THIS CASE
657. C
658. 87 CONTINUE
659. 90 IF(NCASE-20)91,91,94
660. 91 ICASE=0
661.  GO TO 8
662. 94 STOP
663.  END

```



```

1. SUBROUTINE PCOM(NW,NCOM)
2. C *****
3. C PCOM-PRINTS ALL LOCATIONS IN THE COMMON BLOCK
4. C
5. C
6. C NW = LINE PRINTER LOGICAL UNIT NUMBER
7. C NCOM = NUMBER OF LOCATIONS IN COMMON BLOCK
8. C
9. C *****
10. C COMMON VALU(1)
11. C WRITE(NW,2)
12. C 2 FORMAT(/)
13. C WRITE(NW,1) (VALU(I),I=1,100)
14. C 1 FORMAT( 2(10E11.3//),4(10E11.3//),4(10E11.3//) )
15. C WRITE(NW,3) (VALU(I),I=101,NCOM)
16. C 3 FORMAT( 5(10E11.3//) )
17. C RETURN
18. C END

```

```

PCO 002
PCO 003
PCO 004
PCO 005
PCO 006
PCO 007
PCO 008
PCO 009
PCO 010
PCO 011
PCO 012
PCO 013
PCO 014
PCO 015
PCO 016
PCO 018
PCO 019

```

1.	SUBROUTINE EULR6(A,Q)	ER6 0010
2.	COMPUTES EULER PARAMETERS FROM ROTATION MATRIX	ER6 0020
3.	SENSE IS A=TA	ER6 0030
4.	DIMENSION A(9),Q(4)	ER6 0040
5.	X=A(1)+A(5)+A(9)+1.	ER6 0050
6.	IF(X.LT.1E-8.AND.X.GT.-1E-8) X=0.0	
7.	Z4=SQR(X)	
8.	IF(X)10,10,60	ER6 0060
9.	10 D=0.	ER6 0070
10.	X=1.+A(1)-X	ER6 0080
11.	IF(X.LT.1E-8.AND.X.GT.-1E-8) X=0.0	
12.	IF(X)20,20,50	
13.	20 Z1=0.	ER6 0090
14.	X=A(5)+1.	ER6 0100
15.	IF(X.LT.1E-8.AND.X.GT.-1E-8) X=0.0	ER6 0110
16.	IF(X)30,30,40	
17.	30 Z2=0.	ER6 0120
18.	Z3=2.	ER6 0130
19.	GO TO 70	ER6 0140
20.	40 Z2=SQR(2.*X)	ER6 0150
21.	Z3=(A(6)+A(8))/Z2	ER6 0160
22.	GO TO 70	ER6 0170
23.	50 Z1=SQR(2.*X)	ER6 0180
24.	Z2=(A(2)+A(4))/Z1	ER6 0190
25.	Z3=(A(3)+A(7))/Z1	ER6 0200
26.	GO TO 70	ER6 0210
27.	60 Z4=SQR(X)	ER6 0220
28.	Z1=(A(6)-A(8))/Z4	ER6 0230
29.	Z2=(A(7)-A(3))/Z4	ER6 0240
30.	Z3=(A(2)-A(4))/Z4	ER6 0250
31.	70 Q(1)=.5*Z1	ER6 0260
32.	Q(2)=.5*Z2	ER6 0270
33.	Q(3)=.5*Z3	ER6 0280
34.	Q(4)=.5*Z4	ER6 0290
35.	RETURN	ER6 0300
36.	END	ER6 0310
		ER6 0320

```

1. SUBROUTINE EULR5(Q,A) ERS 0010
2. C COMPUTES ROTATION MATRIX FROM EULER PARAMETERS ERS 0020
3. C SENSE IS R=AR* ERS 0030
4. DIMENSION Q(4),A(3,3) ERS 0040
5. P=Q(4)*Q(4)-0.5 ERS 0050
6. DO 50 I=1,3 ERS 0060
7. DO 50 J=1,3 ERS 0070
8. X=Q(I)*Q(J) ERS 0080
9. KGN=2*(J-I) ERS 0090
10. IF(KGN)10,40,-0 ERS 0100
11. 10 SGN=KGN+3 ERS 0110
12. GO TO 30 ERS 0120
13. 20 SGN=KGN-3 ERS 0130
14. 30 KGN=6-I-J ERS 0140
15. X=X+SGN*Q(KGN)*Q(4) ERS 0150
16. GO TO 50 ERS 0160
17. 40 X=X+P ERS 0170
18. 50 A(I,J)=2.0*X ERS 0180
19. RETURN ERS 0190
20. END ERS 0200

```

```

1. SUBROUTINE LOOK1(F,FT,X,XT,NX,IX,MULT) LK1 0010
2. C***** LK1 0020
3. C ONE-DIMENSIONAL TABLE LOOKUP ROUTINE (* = RETURNED VALUES) LK1 0030
4. C C = FT(X) ( ) LK1 0040
5. C C FT FUNCTION TABLE FT(NR) LK1 0050
6. C C NR NO. OF ROWS IN FT-TABLE LK1 0060
7. C C NC NO. OF COLUMNS IN FT-TABLE LK1 0070
8. C C X WORKING VALUE OF INDEPENDENT VARIABLE LK1 0080
9. C C XT INDEPENDENT VARIABLE TABLE LK1 0090
10. C C NX DIMENSION OF XT-TABLE LK1 0100
11. C C *IX X INDEX ON PREVIOUS LOOKUP (UPDATED ON EACH CALL) LK1 0110
12. C C MULT = 0, USE PREVIOUS X LK1 0120
13. C C MULT = 1, LOOK UP NEW X, LK1 0130
14. C C***** LK1 0140
15. C DIMENSION FT(1),XT(1) LK1 0150
16. C IF(MULT-1)2,1,2 LK1 0160
17. C 1 CALL INDEX(X,XT,NX,IX,KEEP,RX) LK1 0170
18. C 2 F=FT(IX) LK1 0180
19. C IF(KEEP-1)3,4,3 LK1 0190
20. C 3 F=(FT(IX+1)-F)*RX+F LK1 0200
21. C 4 RETURN LK1 0210
22. C END LK1 0220

```

```

1. SUBROUTINE LOOK2(F,FT,MR,X,XT,NX,Y,YT,NY,IX,IV,MULT)      LK2 0010
2. C*****                                                    LK2 0020
3. C TWO-DIMENSIONAL TABLE LOOKUP ROUTINE (* = RETURNED VALUES)  LK2 0030
4. C F = FT(X,Y) ( ) LK2 0040
5. C FT FUNCTION TABLE FT(MR,NC) LK2 0050
6. C MR NO. OF ROWS IN FT-TABLE LK2 0060
7. C NC NO. OF COLUMNS IN FT-TABLE LK2 0070
8. C X,Y WORKING VALUES OF INDEPENDENT VARIABLES LK2 0080
9. C XT,YT INDEPENDENT VARIABLE TABLES LK2 0090
10. C NX,NY DIMENSION OF XT,YT TABLES LK2 0100
11. C *IX,IV X,Y INDEXES ON PREVIOUS LOOKUP (UPDATED ON EACH CALL) LK2 0110
12. C MULT = 0, USE PREVIOUS X,Y LK2 0120
13. C MULT = 1, LOOK UP NEW X,Y, LK2 0130
14. C*****                                                    LK2 0140
15. C DIMENSION FT(1),XT(1),YT(1) LK2 0150
16. C IF(MULT-1)2,1,2 LK2 0160
17. C 1 CALL INDEX(Y,YT,NY,IV,KEEP,RY) LK2 0170
18. C I=1+(IV-1)*MR LK2 0180
19. C II=I+MR LK2 0190
20. C 2 CALL LOOK1(F,FT(I),X,XT,NX,IX,MULT) LK2 0200
21. C IF(KEEP-1)3,4,3 LK2 0210
22. C 3 CALL LOOK1(F2,FT(II),X,XT,NX,IX,1) LK2 0220
23. C F=(F2-F)*RY+F LK2 0230
24. C 4 RETURN LK2 0240
25. C END LK2 0250

```

```

1. SUBROUTINE INDEX(X,XT,NX,IX,KEEP,RATIO) IND 0010
2. C***** IND 0020
3. C TABLE INDEX LOOKUP ROUTINE (* = RETURNED VALUES) IND 0030
4. C X WORKING VALUE OF INDEPENDENT VARIABLES IND 0040
5. C XT INDEPENDENT VARIABLE TABLE XT(NX) IND 0050
6. C NX DIMENSION OF X-TABLE IND 0060
7. C IX INDEX OF PREVIOUS LOOKUP (UPDATED ON EACH CALL) IND 0070
8. C *KEEP = 0 - X.NE.ANY XT. INTERPOLATION WAS REQUIRED. IND 0080
9. C = 1 - X.EQ.XT(IX). INTERPOLATION NOT REQUIRED. IND 0090
10. C *RATIO. INTERPOLATION RATIO IND 0100
11. C***** IND 0110
12. DIMENSION XT(1) IND 0120
13. IX=0
14. RATIO=0. IND 0130
15. KEEP=0 IND 0140
16. IF(NX-IX)1,1,2 IND 0150
17. 1 IX=NX-1 IND 0160
18. 2 IF(IX-1)3,3,4 IND 0170
19. 3 IX=1 IND 0180
20. 4 IF(NX-1)10,10,5 IND 0190
21. 5 IF(XT(IX)-X)6,10,7 IND 0200
22. 6 IF(XT(IX+1)-X)8,9,11 IND 0210
23. 7 IX=IX-1 IND 0220
24. 8 IF(IX-1)9,5,5 IND 0230
25. 9 IX=IX+1 IND 0240
26. 10 IF(IX-NX)5,10,10 IND 0250
27. 9 IX=IX+1 IND 0260
28. 10 KEEP=1 IND 0270
29. RETURN IND 0280
30. 11 RATIO=(X-XT(IX))/(XT(IX+1)-XT(IX)) IND 0290
31. RETURN IND 0300
32. END IND 0310

```


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1.	SUBROUTINE ZCOM (NCOM)	ZCO 001
2.	C*****	ZCO 003
3.	C	ZCO 004
4.	C SUBROUTINE TO ZERO ALL LOCATIONS IN COMMON BLOCK	ZCO 005
5.	C	ZCO 006
6.	C NCOM = NUMBER OF LOCATIONS OF COMMON BLOCK	ZCO 007
7.	C	ZCO 008
8.	C*****	ZCO 009
9.	COMMON VALU(1)	ZCO 010
10.	DO 10 I=1,NCOM	ZCO 011
11.	10 VALU(I)=0.	ZCO 012
12.	RETURN	ZCO 013
13.	END	


```

1. SUBROUTINE TWIST(THETA,T,N) TWI 001
2. C***** TWI 002
3. C TWI 003
4. C TWIST COMPUTES THE TRANSFORMATION MATRIX-T FOR A ROTATION ABOUT TWI 004
5. C ONE OF THE 3 AXES IN THE SENSE TWI 005
6. C TWI 006
7. C R = T R' TWI 007
8. C TWI 008
9. C THETA = ANGLE OF ROTATION, IN RADIANS TWI 009
10. C T = 3X3 ROTATION MATRIX-OUTPUT TWI 010
11. C N = AXIS NO. FOR WHICH ROTATION IS CALLED (1,2 OR 3) TWI 011
12. C TWI 012
13. C***** TWI 013
14. C DIMENSION T(3,3) TWI 014
15. C ZERO=0. TWI 015
16. C ONE=1. TWI 016
17. C CTHET= COS(THETA) TWI 017
18. C DO 90 I=1,3 TWI 018
19. C DO 90 J=1,3 TWI 019
20. C IF(I-J)10,60,10 TWI 020
21. C 10 IF((I-N)*(J-N))30,20,30 TWI 021
22. C 20 X=ZERO TWI 022
23. C GO TO 50 TWI 023
24. C 30 X= SIN(THETA) TWI 024
25. C IF(N-2)50,40,50 TWI 025
26. C 40 X=-X TWI 026
27. C 50 T(I,J)=-X TWI 027
28. C GO TO 90 TWI 028
29. C 60 IF(I-N)70,80,70 TWI 029
30. C 70 X=CTHET TWI 030
31. C GO TO 90 TWI 031
32. C 80 X=ONE TWI 032
33. C 90 T(J,I)=X TWI 033
34. C RETURN TWI 034
35. C END TWI 035

```

```

1. SUBROUTINE AUTO(X,E,KONTROL)
2. DIMENSION X(40),E(40)
3. ERW=SQRT(E(1)*E(1)+E(2)*E(2)+E(3)*E(3))
4. ERQ=SQRT(E(4)*E(4)+E(5)*E(5)+E(6)*E(6)+E(7)*E(7))
5. ERV=SQRT(E(8)*E(8)+E(9)*E(9)+E(10)*E(10))
6. ERR=SQRT(E(11)*E(11)+E(12)*E(12)+E(13)*E(13))
7. ER=SQRT(ERW*ERW+ERQ*ERQ)
8. KONTROL=1
9. IF(ER.GT.32.E-5)KONTROL=2
10. IF(ER.LE..5E-5)KONTROL=3
11. RETURN
12. END

```


53.	110	FORMAT(6(2X,A4,E14.8))	
54.		RETURN	BL0 020
55.		END	BL0 029
			BL0 030

```

1. SUBROUTINE MINV(A,N,D,L,M) MIN 0001
2. C***** MIN 0002
3. C MIN 0003
4. C MATRIX INVERSE, OF AN N*M MATRIX-A INTO THE SAME MATRIX-A MIN 0004
5. C MIN 0005
6. C -1 D - OUTPUT DETERMINANT OF ORIGINAL A MIN 0006
7. C A = A L, M ARE TWO WORKING INTEGER VECTORS MIN 0007
8. C MIN 0008
9. C MIN 0009
10. C NOTE THAT THE ORIGINAL A-MATRIX IS DESTROYED MIN 0010
11. C ALSO NOTE THAT A CHECK ON D SHOULD BE MADE IN CASE MATRIX-A EVER MIN 0011
12. C BECOMES SINGULAR MIN 0012
13. C***** MIN 0013
14. C DIMENSION A(1),L(1),M(1) MIN 0014
15. C SEARCH FOR LARGEST ELEMENT MIN 0015
16. C D=1.0 MIN 0016
17. C MK=M MIN 0017
18. C DO 80 K=1,M MIN 0018
19. C L(K)=K MIN 0019
20. C M(K)=K MIN 0020
21. C KK=MK+K MIN 0021
22. C BIGA=A(KK) MIN 0022
23. C DO 20 J=K,M MIN 0023
24. C IZ=M*(J-1) MIN 0024
25. C DO 20 I=K,M MIN 0025
26. C IJ=IZ+I MIN 0026
27. C IF(ABS(BIGA)-ABS(A(IJ))) 15,20,20 MIN 0027
28. C 15 BIGA=A(IJ) MIN 0028
29. C L(K)=I MIN 0029
30. C M(K)=J MIN 0030
31. C 20 CONTINUE MIN 0031
32. C INTERCHANGE ROWS MIN 0032
33. C J=L(K) MIN 0033
34. C IF(J=K) 35,35,25 MIN 0034
35. C 25 KI=K-N MIN 0035
36. C DO 30 I=1,M MIN 0036
37. C KI=KI+N MIN 0037
38. C HOLD=-A(KI) MIN 0038
39. C JI=KI-K+J MIN 0039
40. C A(KI)=A(JI) MIN 0040
41. C 30 A(JI)=HOLD MIN 0041
42. C INTERCHANGE COLUMNS MIN 0042
43. C 35 I=M(K) MIN 0043
44. C IF(I=K) 45,45,38 MIN 0044
45. C 38 JP=M*(I-1) MIN 0045
46. C DO 40 J=1,M MIN 0046
47. C JK=MK+J MIN 0047
48. C JI=JP+J MIN 0048
49. C HOLD=-A(JK) MIN 0049
50. C A(JK)=A(JI) MIN 0050
51. C MIN 0051
52. C MIN 0052

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53. 40 A(JI) = HOLD MIN 0053
54. C DIVIDE COLUMN BY MINUS PIVOT (VALUE OF PIVOT ELEMENT IS MIN 0054
55. C CONTAINED IN BIGA) MIN 0055
56. 45 IF(ABS(BIGA)-1.5-20)46,46,48 MIN 0056
57. 46 D=0.0 MIN 0057
58. RETURN MIN 0058
59. 48 DO 55 I=1,N MIN 0059
60. IF(I-K) 50,55,50 MIN 0060
61. 50 IK=IK+I MIN 0061
62. A(IK)=A(IK)/(-BIGA) MIN 0062
63. 55 CONTINUE MIN 0063
64. C REDUCE MATRIX MIN 0064
65. DO 65 I=1,N MIN 0065
66. IK=IK+I MIN 0066
67. HOLD=A(IK) MIN 0067
68. IJ=I-N MIN 0068
69. DO 65 J=1,N MIN 0069
70. IJ=IJ+N MIN 0070
71. IF(I-K) 60,65,60 MIN 0071
72. 60 IF(J-K) 62,65,62 MIN 0072
73. 62 KJ=IJ-I+K MIN 0073
74. A(IJ)=HOLD*A(KJ)+A(IJ) MIN 0074
75. 65 CONTINUE MIN 0075
76. C DIVIDE ROW BY PIVOT MIN 0076
77. KJ=K-N MIN 0077
78. DO 75 J=1,N MIN 0078
79. KJ=KJ+N MIN 0079
80. IF(J-K) 70,75,70 MIN 0080
81. 70 A(KJ)=A(KJ)/BIGA MIN 0081
82. 75 CONTINUE MIN 0082
83. C PRODUCT OF PIVOTS MIN 0083
84. D=D*BIGA MIN 0084
85. C REPLACE PIVOT BY RECIPROCAL MIN 0085
86. A(KK)=1.0/BIGA MIN 0086
87. 80 CONTINUE MIN 0087
88. C FINAL ROW AND COLUMN INTERCHANGE MIN 0088
89. K=N MIN 0089
90. 100 K=(K-I) MIN 0090
91. IF(K) 150,150,105 MIN 0091
92. 105 I=L(K) MIN 0092
93. IF(I-K) 120,120,108 MIN 0093
94. 108 JQ=N*(K-I) MIN 0094
95. JR=N*(I-I) MIN 0095
96. DO 110 J=1,N MIN 0096
97. JK=JQ+J MIN 0097
98. HOLD=A(JK) MIN 0098
99. JI=JR+J MIN 0099
100. A(JK)=A(JI) MIN 0100
101. 110 A(JI)=HOLD MIN 0101
102. 120 J=N(K) MIN 0102
103. IF(J-K) 100,100,125 MIN 0103
104. 125 KI=K-N MIN 0104

```

105.	DO 130 I=1,N	MIN 0105
106.	KI=KI+N	MIN 0106
107.	HOLD=A(KI)	MIN 0107
108.	J1=KI-K+J	MIN 0108
109.	A(KI)=A(J1)	MIN 0109
110.	130 A(J1)=HOLD	MIN 0110
111.	GO TO 100	MIN 0111
112.	150 RETURN	MIN 0112
113.	END	MIN 0113

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1. SUBROUTINE RUNK2(KUTTA,N)
2. REAL NINE
3. DIMENSION C1(40),C2(40),C3(40),C4(40),C5(40),S1(40),E(40)
4. COMMON TIME,DT,DTP,DTSAN,TRUB,TEND,PCOUM(14)
5. COMMON XD(40)
6. COMMON X(40)
7. DATA HALF,THIRD,SIXTH,EIGHTH,.5,.3333333,.16666667,.125/
8. DATA TWO,THREE,FOUR,EIGHT,NINE,THIRTY/2.,3.,4.,8.,9.,30./
9. GO TO (1,2,3,4,5),KUTTA
10. 1 DO 11 I=1,N
11. SX(I)=X(I)
12. C1(I)=DT*XD(I)
13. 11 X(I)=SX(I)+THIRD*C1(I)
14. RETURN
15. 2 DO 12 I=1,N
16. C2(I)=DT*SX(I)
17. 12 X(I)=SX(I)+SIXTH*(C1(I)+C2(I))
18. RETURN
19. 3 DO 13 I=1,N
20. C3(I)=DT*XD(I)
21. 13 X(I)=SX(I)+EIGHTH*(C1(I)+THREE*C3(I))
22. RETURN
23. 4 DO 14 I=1,N
24. C4(I)=DT*XD(I)
25. 14 X(I)=SX(I)+HALF*(C1(I)-THREE*C3(I)+FOUR*C4(I))
26. RETURN
27. 5 DO 15 I=1,N
28. C5(I)=DT*XD(I)
29. X(I)=SX(I)+SIXTH*(C1(I)+FOUR*C4(I)+C5(I))
30. 15 E(I)=(TWO*C1(I)-NINE*C3(I)+EIGHT*C4(I)-C5(I))/THIRTY*(DT/.25)
31. CALL AUTO(X,E,KONTRL)
32. IF(KONTRL-2)10,20,30
33. 20 DT=DT*HALF
34. 00 21 I=1,N
35. 21 X(I)=SX(I)
36. KUTTA=0
37. RETURN
38. 10 TIME=TIME+DT
39. RETURN
40. 30 TIME=TIME+DT
41. DT=DT*TWO
42. RETURN
43. END

```


REFERENCES

1. Shuford, D. W.: "Users Guide for Program REENTR; Space Shuttle External Tank Reentry Simulation Program." Northrop Services, Inc., Huntsville, Alabama, M-250-1303, August 1974.

BIBLIOGRAPHY

Crenshaw, J.: "QUAD2 Integration Routine." Northrop Services, Inc., Huntsville, Alabama, Informal Memorandum 7960-69-1, January 1969.

Grafton, E. A. and Javinen, W. A.: "Users Guide: SRB Reentry Program 'BDBI'." Northrop Services, Inc., Huntsville, Alabama, TN-250-1329, September 1974.

APPROVAL

USERS GUIDE FOR SKYLAB DYNAMICS PROGRAM, SKYDYN

by M. S. Hopkins

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